

GW Detector Subsystems I & II

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Topics

Anamaria:

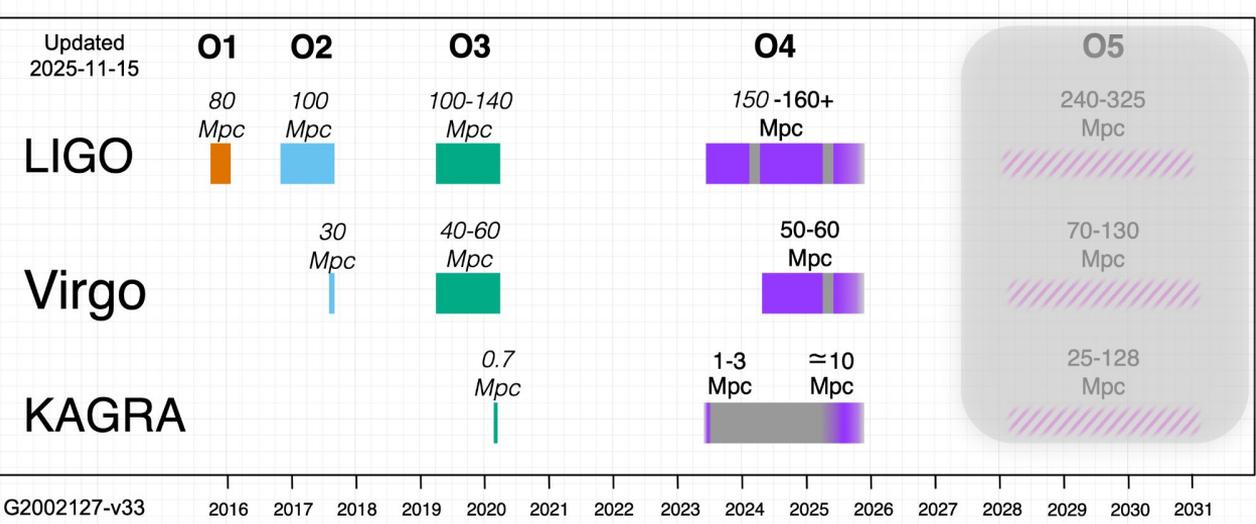
- Some LIGO history
- Michelson ifos
- LSC
- ISI and SUS
- PEM
- Noise budgeting

Nikhil:

- PSL
- IOO
- CDS
- ASC
- Control loops

Brief LIGO history

- ❖ First concept: R. Drever, K. Thorne, R. Weiss 1980's
- ❖ Funded by NSF 1992
- ❖ Construction finished circa 2000
- ❖ Initial LIGO era: 2002-2009
- ❖ Advanced LIGO: finished installation 2014
- ❖ First detection: Sep 14 2015



<https://observing.docs.ligo.org/plan/>



M. Fyffe

How does a Michelson interferometer detect gravitational waves



Simple Michelson

$$E_x = -\frac{1}{\sqrt{2}}r_x E_{in} e^{2ikl_x}, \quad E_y = \frac{1}{\sqrt{2}}r_y E_{in} e^{2ikl_y}$$

$$E_{as} = \frac{1}{\sqrt{2}}(E_x + E_y) = \frac{1}{2}E_{in}(r_y e^{2ikl_y} - r_x e^{2ikl_x})$$

$$P_{as} = |E_{as}|^2 = \frac{1}{4}P_{in}[(r_x - r_y)^2 + 4r_x r_y \sin(k(l_x - l_y))]$$

dark fringe (min): $P_{as} = \frac{1}{4}P_{in}(r_x - r_y)^2$

bright fringe (max) : $P_{as} = \frac{1}{4}P_{in}(r_x + r_y)^2$

-redefine with $\Delta l = l_x - l_y$ and $l = \frac{l_x + l_y}{2}$

$$E_{as} = -\frac{1}{2}E_{in}e^{i2kl}(r_x e^{ik\Delta L} - r_y e^{-ik\Delta L})$$

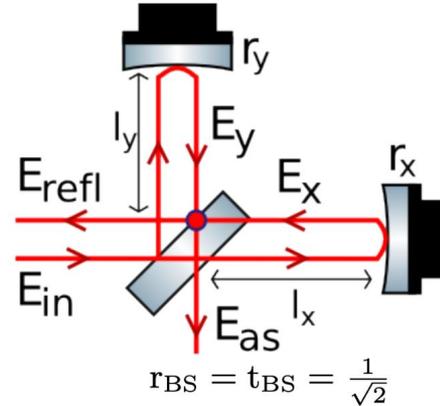
$$E_{as} = -\frac{1}{2}E_{in}e^{i2kl}((r_x - r_y)\cos(k\Delta L) + i(r_x + r_y)\sin(k\Delta L))$$

$$E_{as} \approx -E_{in}ie^{i2kl}\sin(k\Delta L)$$

-the effect of a GW is only on $\Delta L \rightarrow \Delta L + 2hl$

$$P_{as} = |E_{as}|^2 \sim \sin^2(k\Delta L + 2khl) \sim \sin^2(k\Delta L) + \sin(2k\Delta L)2khl$$

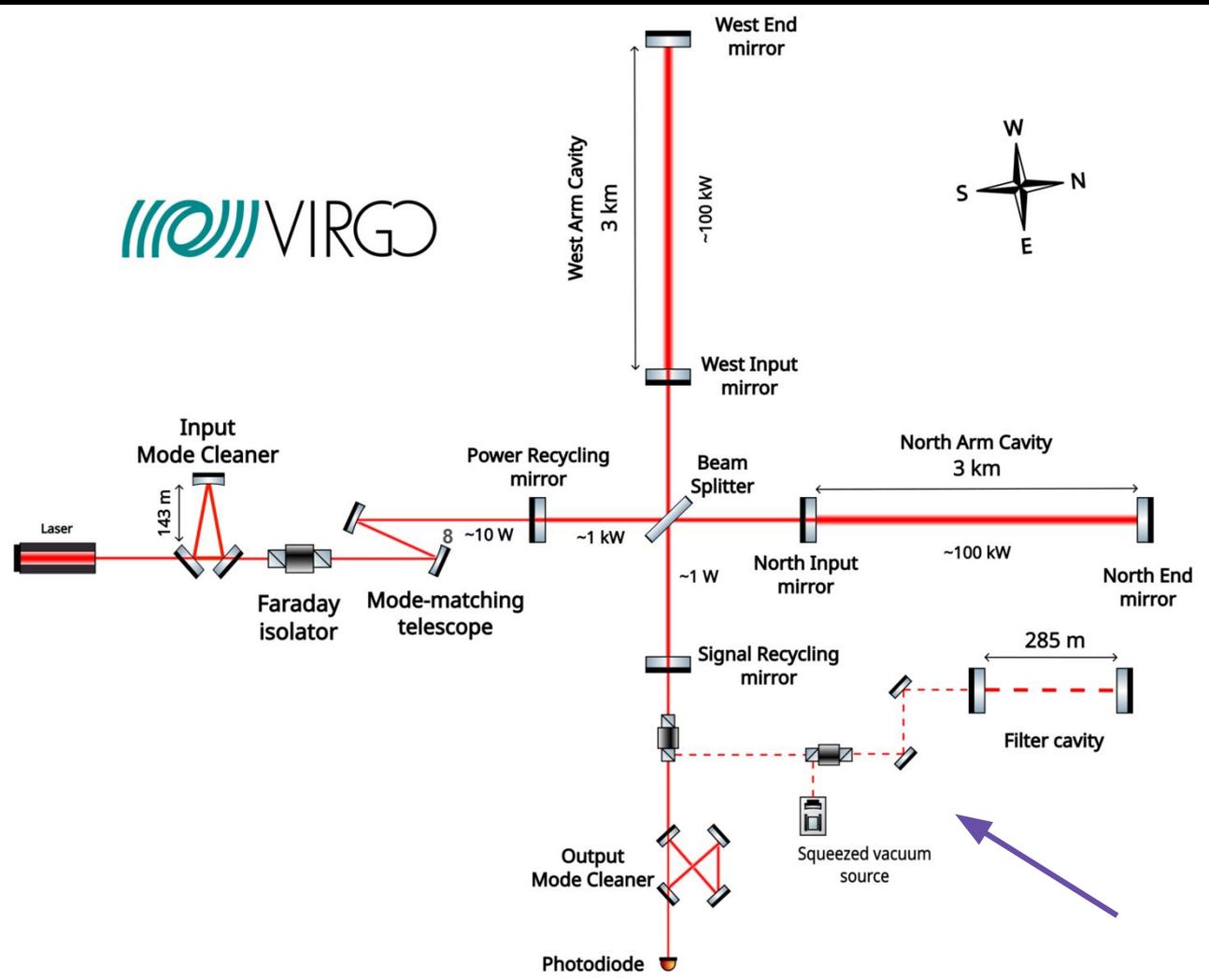
if ΔL is 0, we see no signal to first order ?! \implies we need Schnupp
assymetry, a macroscopic length difference between arms



[G1400346](#)

More realistic layout

Virgo has a similar layout, biggest difference is a few lengths and non-folded recycling cavities



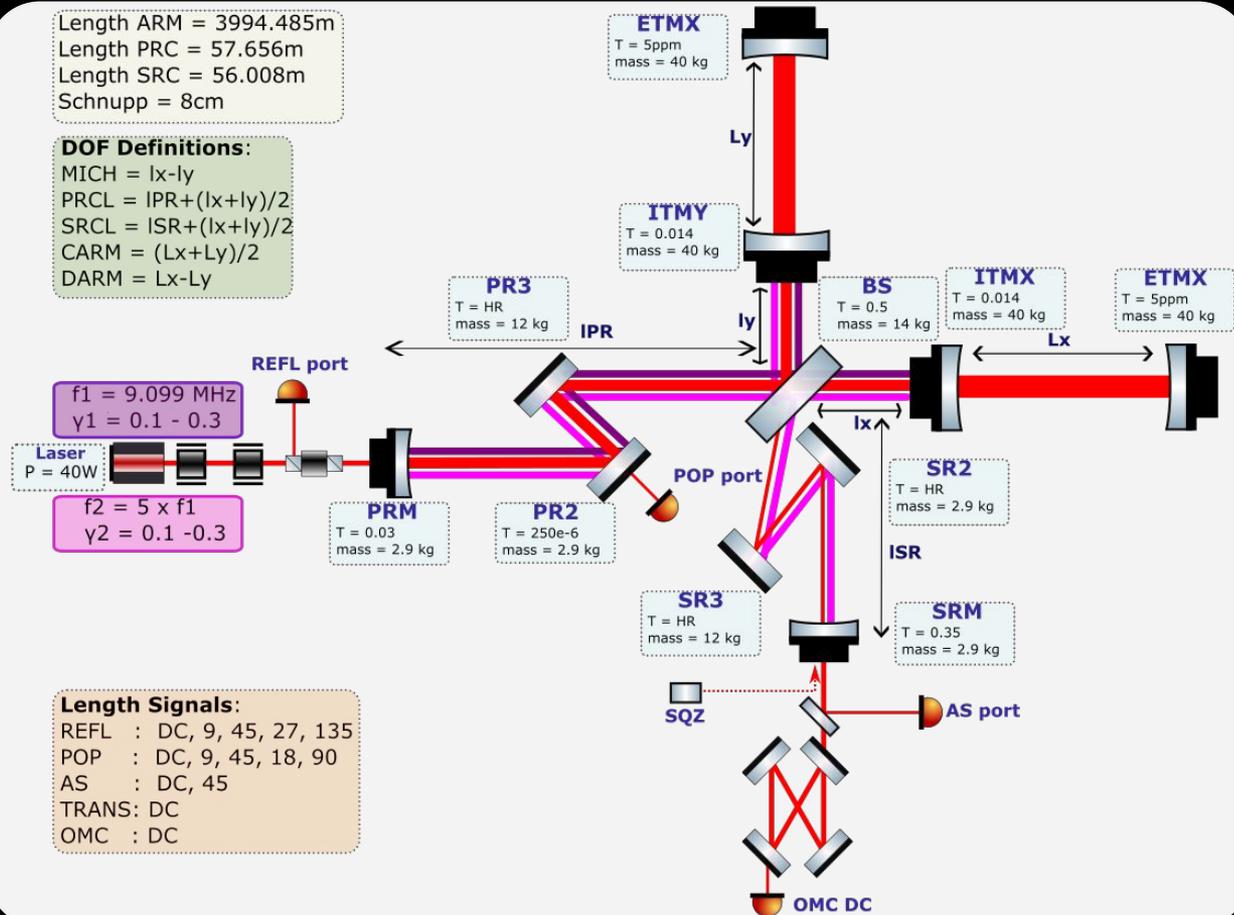
How do we control all these Degrees of Freedom (DoF's)

LIGO has 5 main lengths to control (angular DoF's covered later)

Use RF modulations to extract various signals at a few pick-off ports (~PDH)

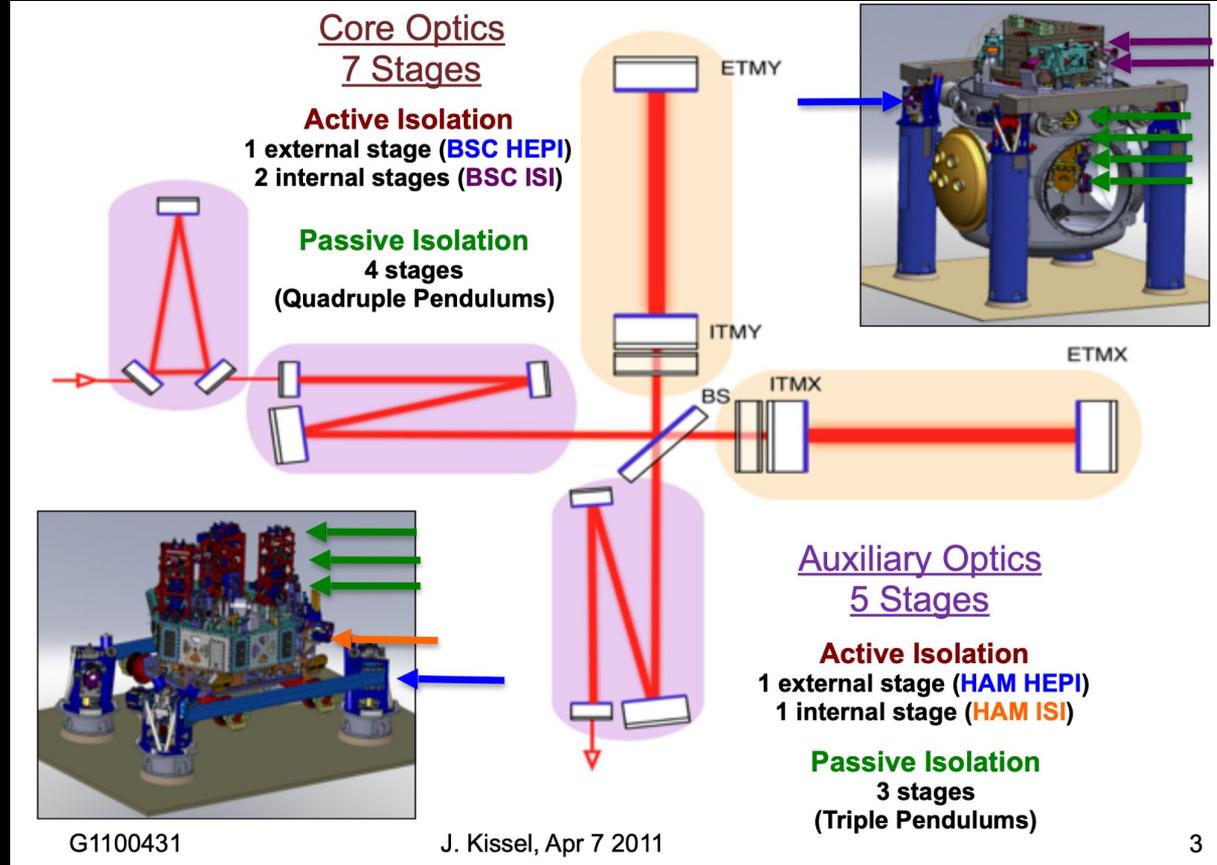
Measure the sensing strength at each port and choose strongest or some diagonalization

Some natural diagonalization common versus differential



Seismic Isolation

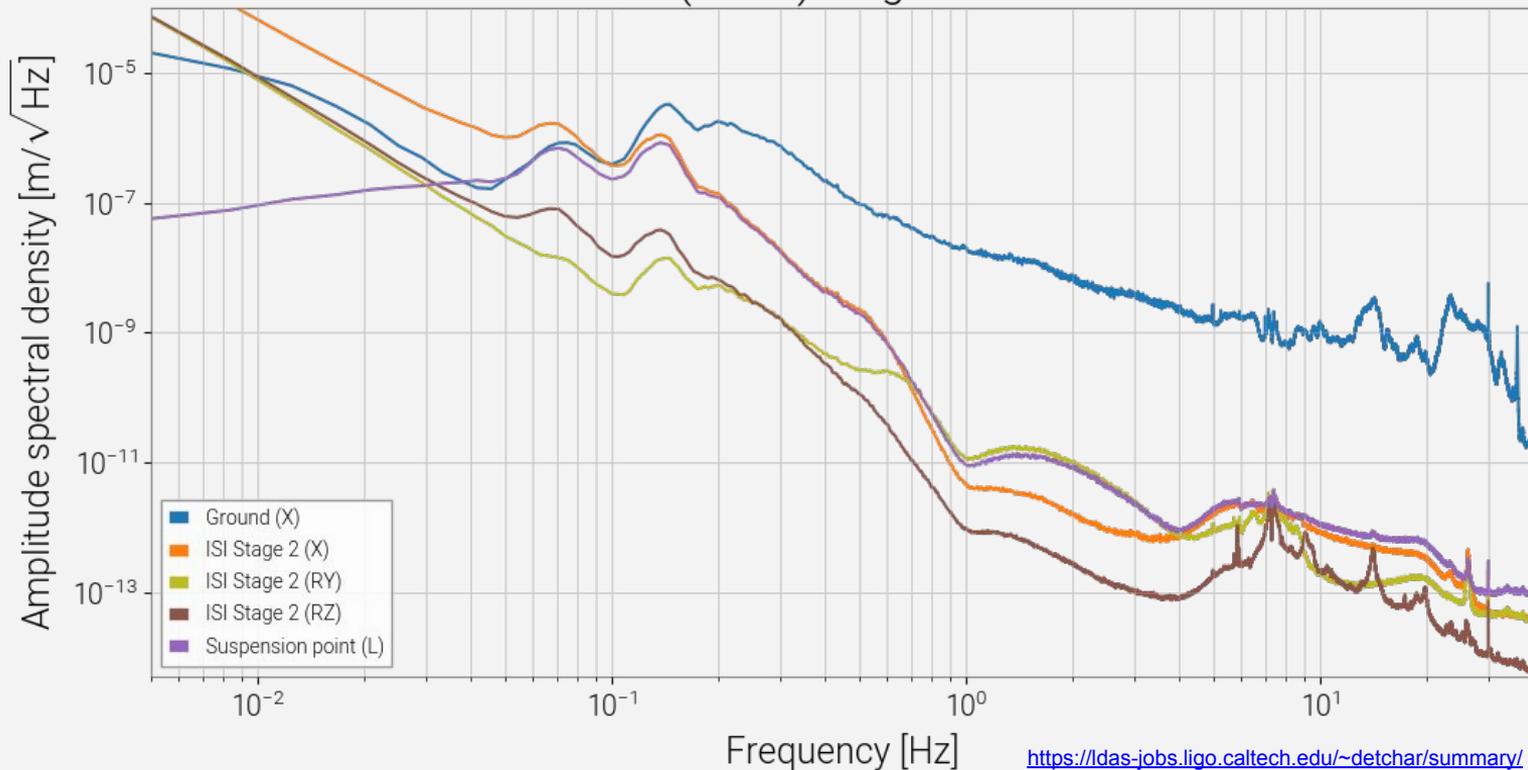
- LIGO has two types:
 - HAM one stage table
 - BSC two-stage table
- Active isolation
 - Several types of sensors and actuators



How well does BSC (2-stage) isolate?

[1446854418-1446940818, state: Isolated]

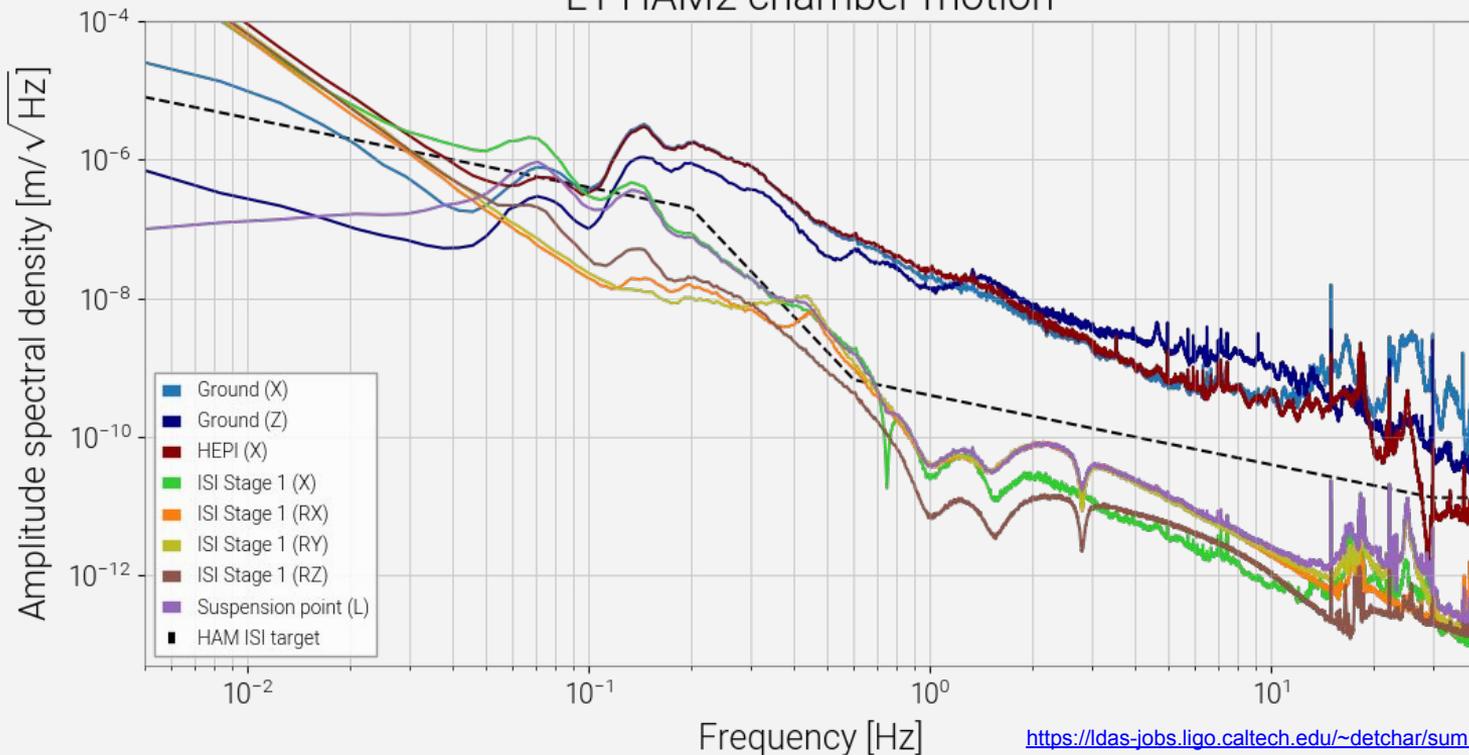
L1 ETMX (BSC4) longitudinal motion



How well does HAM (1-stage) isolate?

[1446854418-1446940818, state: Isolated]

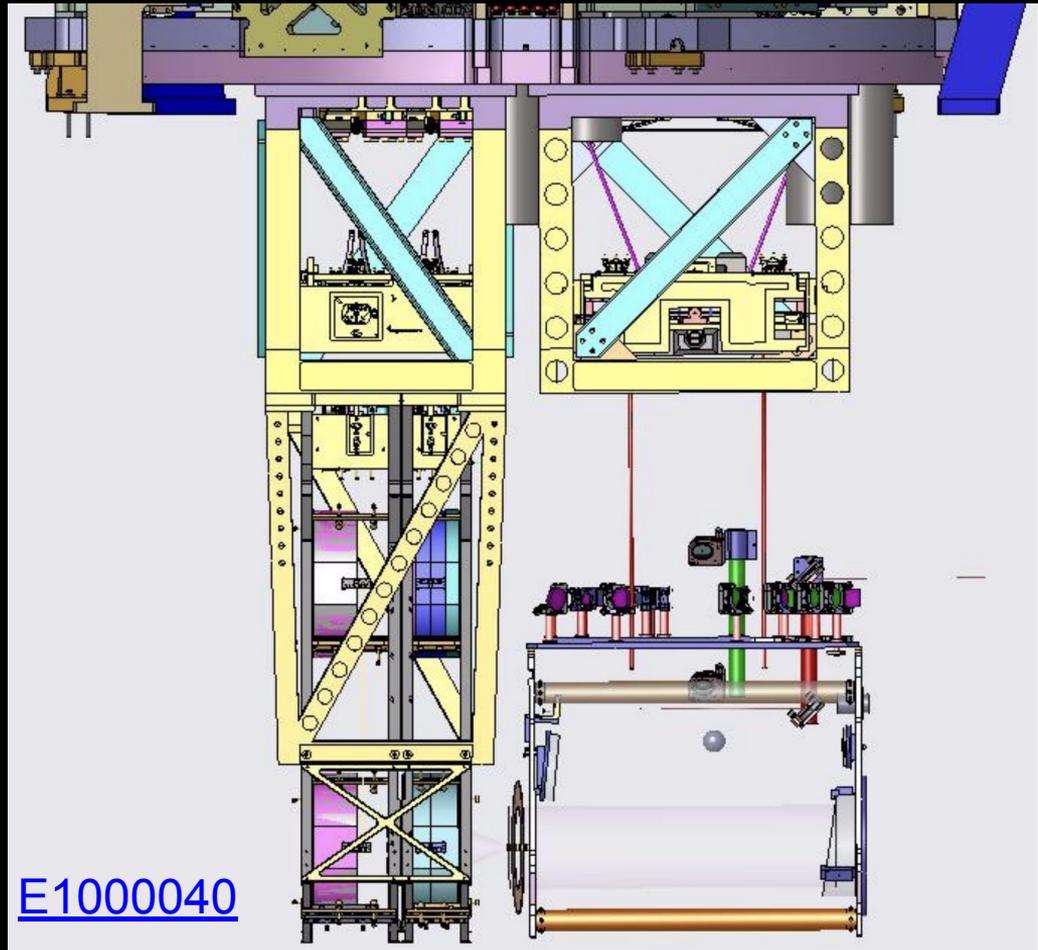
L1 HAM2 chamber motion



<https://lhas-jobs.ligo.caltech.edu/~detchar/summary>

Suspensions - fewest pendula needed

- Each pendulum gives a $1/f^2$
- Complexity depends on isolation needed
- Main/arm optics are quadruple suspensions with a quadruple reaction chain
- Other optics (PRC/SRC) are triples
- Even have double and single for sensing



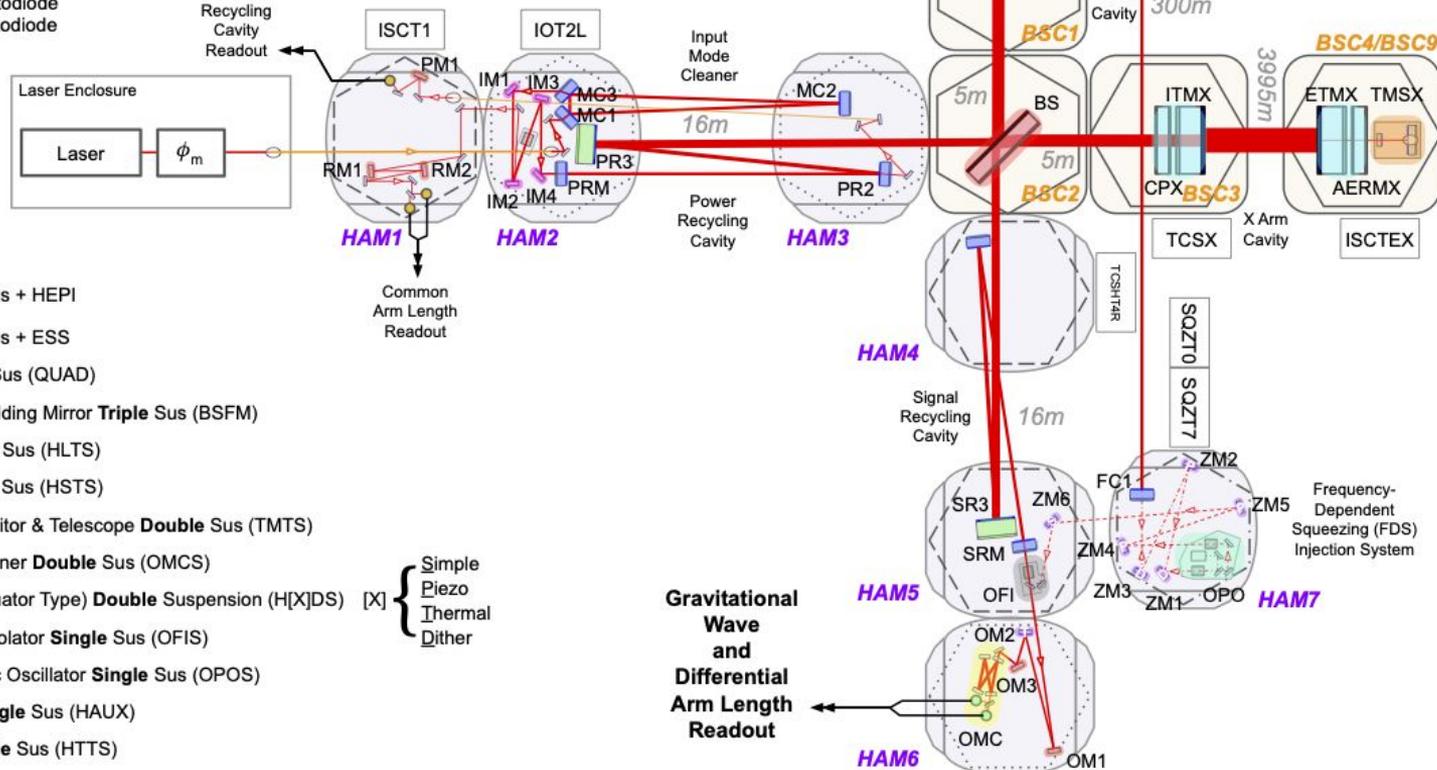
[E1000040](#)

Motion Isolation (seismic tables and suspensions)

- Main Beam
- Elevated Main Beam
- Squeezed Beam
- Collinear Beam

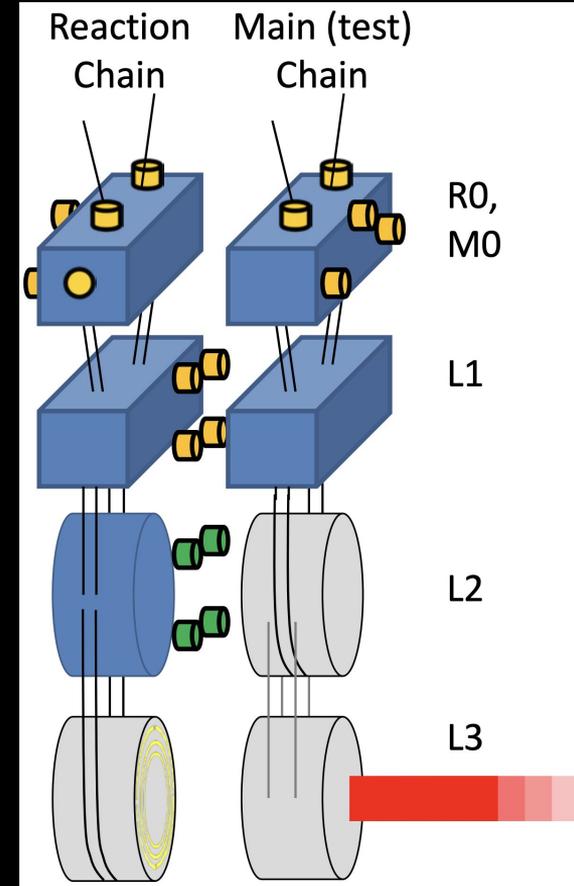
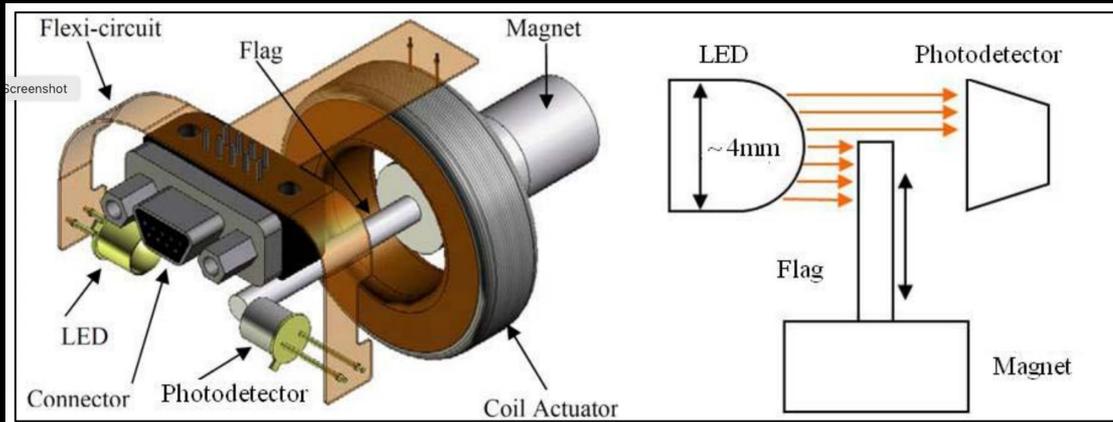
- Periscope
- Fixed Optic
- Radio-Frequency Photodiode
- Audio-Frequency Photodiode

- BSC ISI + HEPI
- HAM ISI + HEPI
- HAM ISI + FF L4Cs + HEPI
- HAM ISI + FF L4Cs + ESS
- Test Mass **Quad** Sus (QUAD)
- Beam Splitter / Folding Mirror **Triple** Sus (BSFM)
- HAM Large **Triple** Sus (HLTS)
- HAM Small **Triple** Sus (HSTS)
- Transmission Monitor & Telescope **Double** Sus (TMTS)
- Output Mode Cleaner **Double** Sus (OMCS)
- HAM (X = M2 Actuator Type) **Double** Suspension (H[X]DS) [X] $\left\{ \begin{array}{l} \text{Simple} \\ \text{Piezo} \\ \text{Thermal} \\ \text{Dither} \end{array} \right.$
- Output Faraday Isolator **Single** Sus (OFIS)
- Optical Parametric Oscillator **Single** Sus (OPOS)
- HAM Auxiliary **Single** Sus (HAUX)
- HAM Tip-Tilt **Single** Sus (HTTS)



Suspension Control

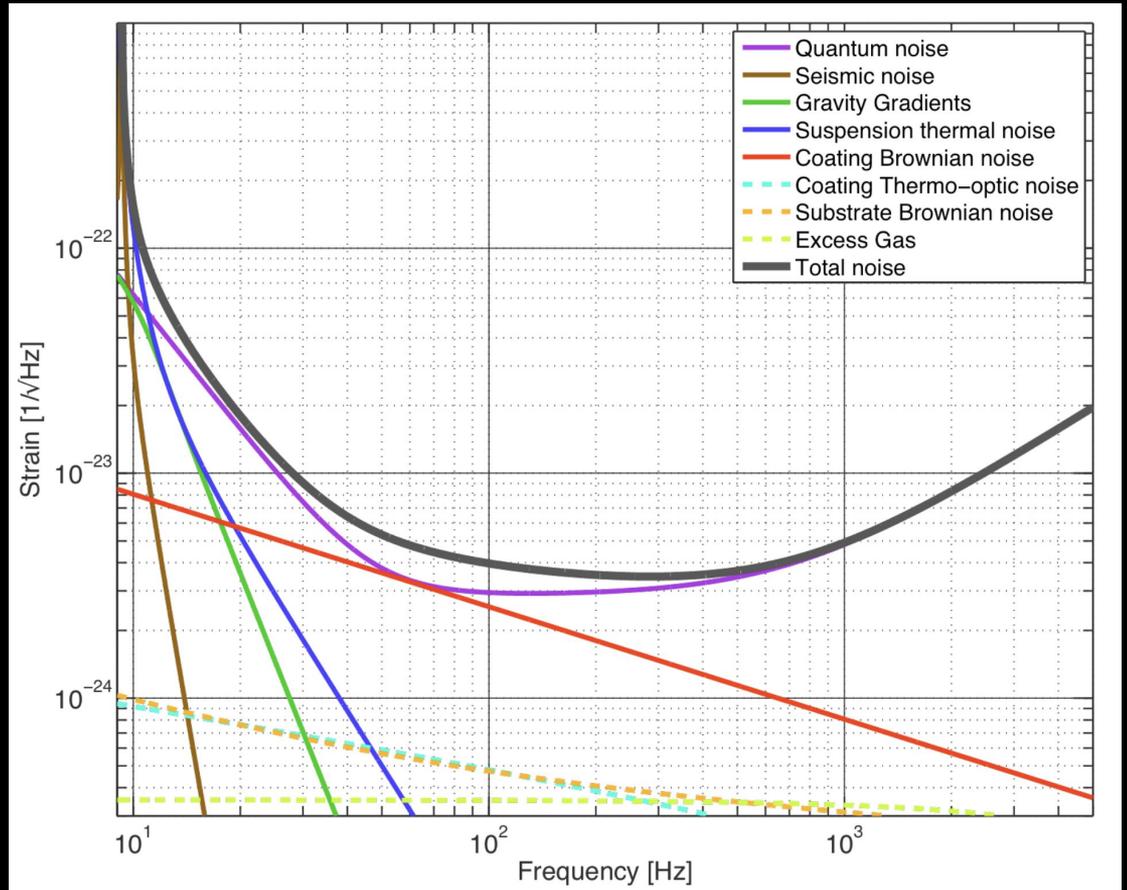
- Most suspensions have OSEMs (optical sensing and electromagnetic actuation) = shadow sensor + coil-magnet
- Test mass has ESD (electrostatic drive) at the bottom
- Some controls are in-between chains
- Each stage has to have quiet actuation
 - I.e. the lower we go, the less range
- Sensor noise matters!
 - Can only damp at the top
 - Coming soon: better sensors!



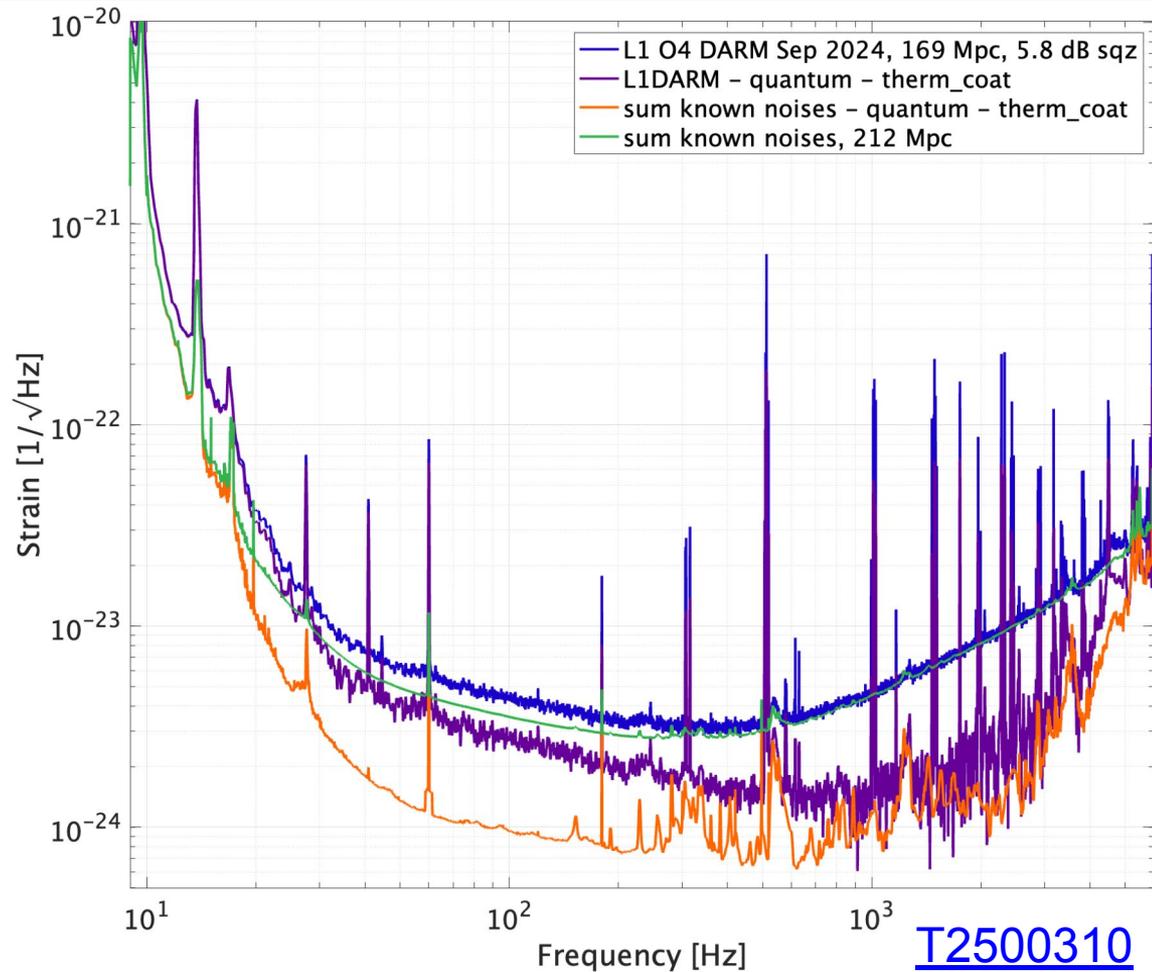
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Fundamental noise sources

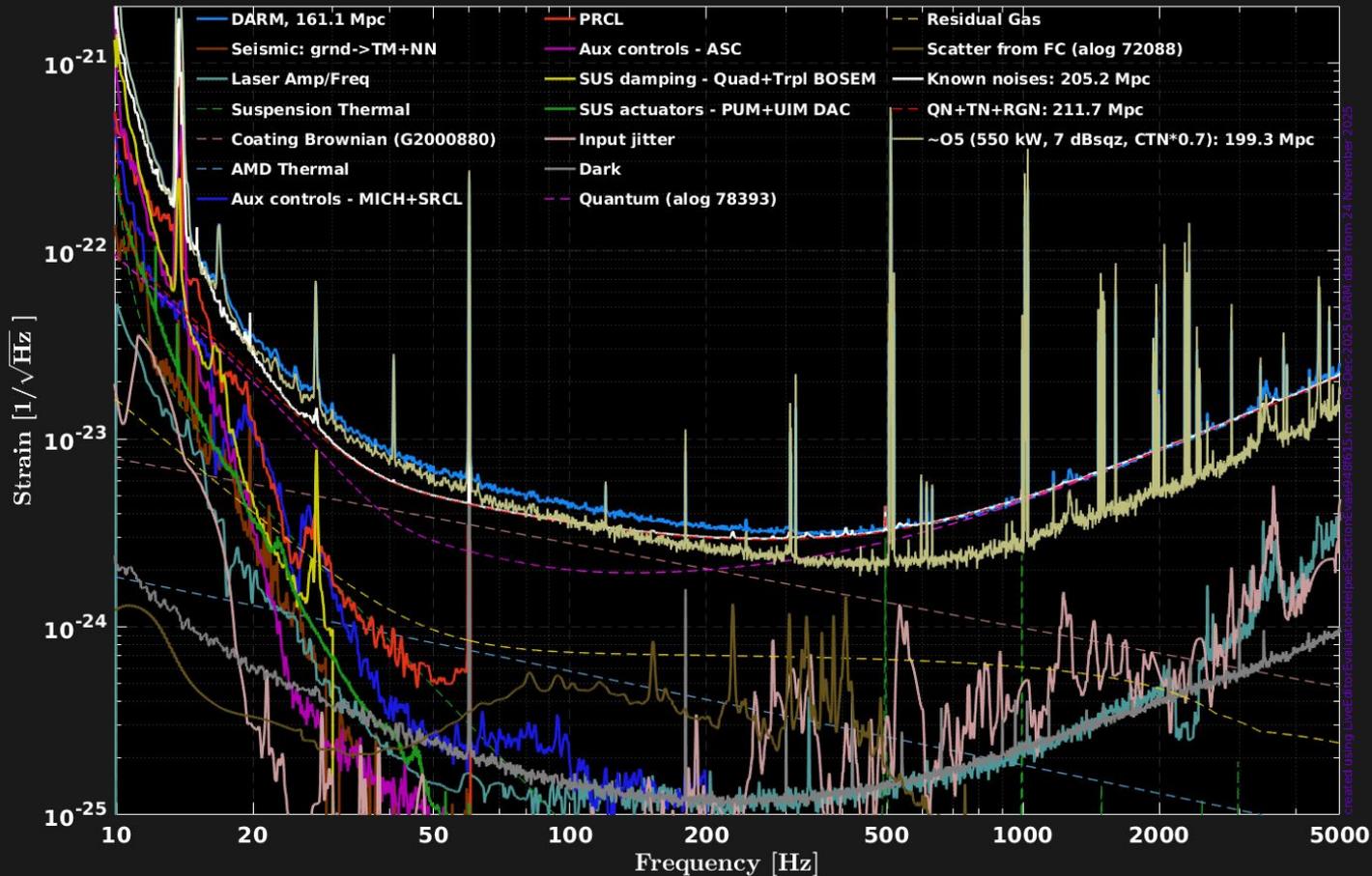
- Thermal noise
 - Trying to push this down for O5 with new test mass coatings
- Quantum noise
 - More power and more squeezing
 - Radiation pressure at low frequency
- Seismic noise
- Gravity Gradient (newtonian noise)
 - Not yet seen
- Residual gas noise
 - Keep vacuum good



Other noise?



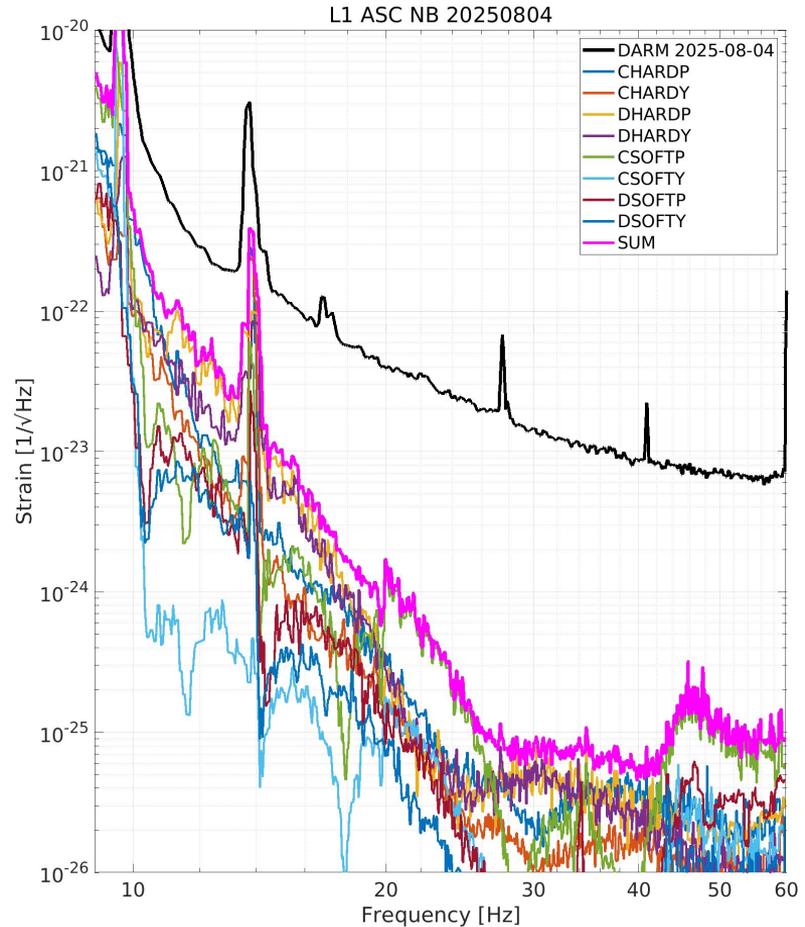
Technical noise sources



V.Frolov
[Alog 79720](#)

Example: ASC breakdown

- Measure each of a type of noise and add in quadrature
- Careful not to double count!



How to measure: injection methods

- Main idea: inject relevant noise, have relevant witness, measure the “transfer function” and then apply it to ambient witness noise
- Transfer functions require coherence, so maybe measure “power-to-power”
 - The difference can tell you the non-linearity of the coupling
 - The scaling can be linear even if the coupling is not
- Is the witness actually relevant?
 - Many channels see injections, but they’re not causally involved
- Is the witness noise the same noise that affects DARM?
 - Eg if limited by sensor noise, then it’s not
- Up/downconversion - eg scatter fringe wrapping

$$CF(f) = \sqrt{\frac{[Y_{inj}(f)]^2 - [Y_{bkg}(f)]^2}{[X_{inj}(f)]^2 - [X_{bkg}(f)]^2}}$$

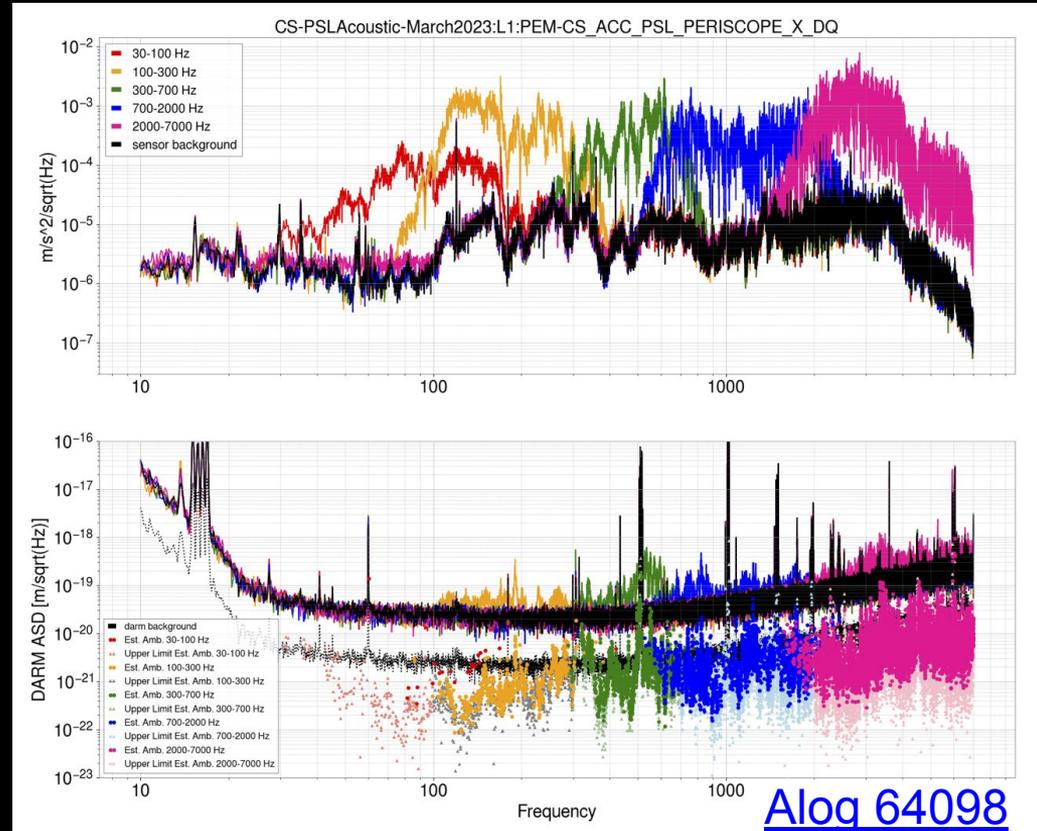
DARM_noise(f) =
CF(f) * Xbkg(f) (1)

[O3 pem paper](#)

where $X_{bkg}(f)$ and $X_{inj}(f)$ are the ASDs of the witness sensor at background and injection times, respectively, and $Y_{bkg}(f)$ and $Y_{inj}(f)$ are the ASDs of DARM at background and injection times. We use *coupling factor* to refer to the value of a coupling function at a single frequency bin.

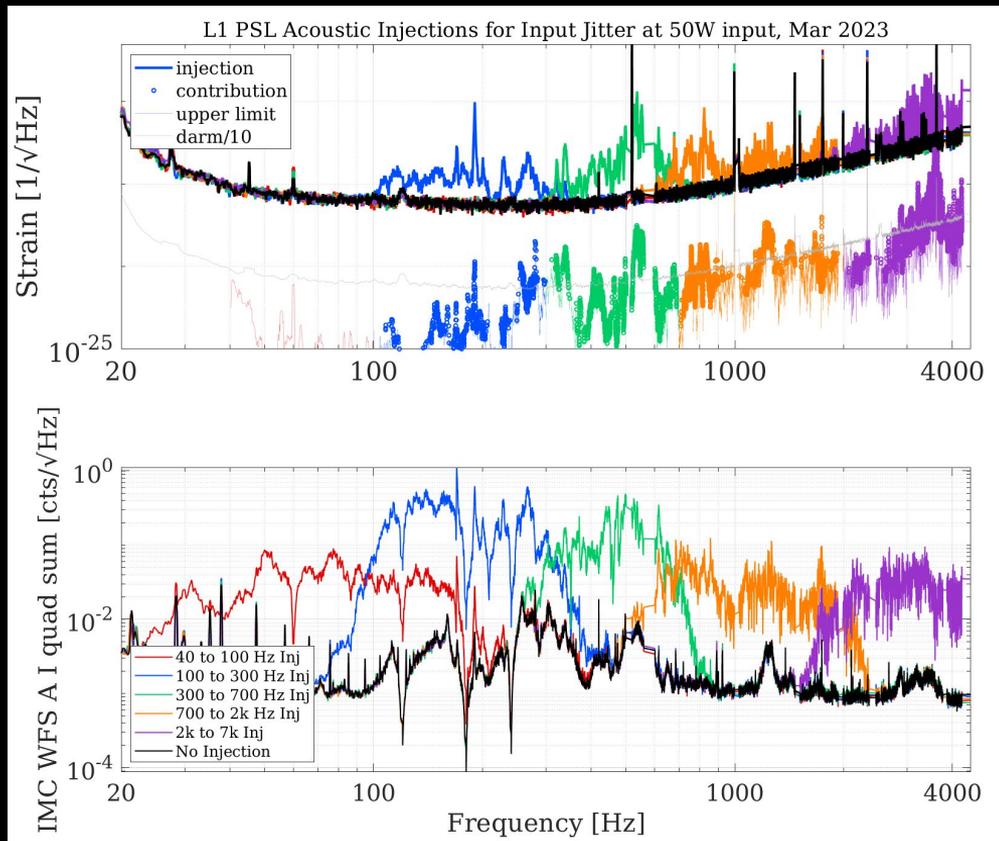
Example: Measuring Input Jitter

- Inject acoustics
 - Few bands to focus power
 - Low-freq use piezo
 - Could use shaker or other injectors
- What sensor to use?
 - PSL periscope is good, others are not
 - But can find better



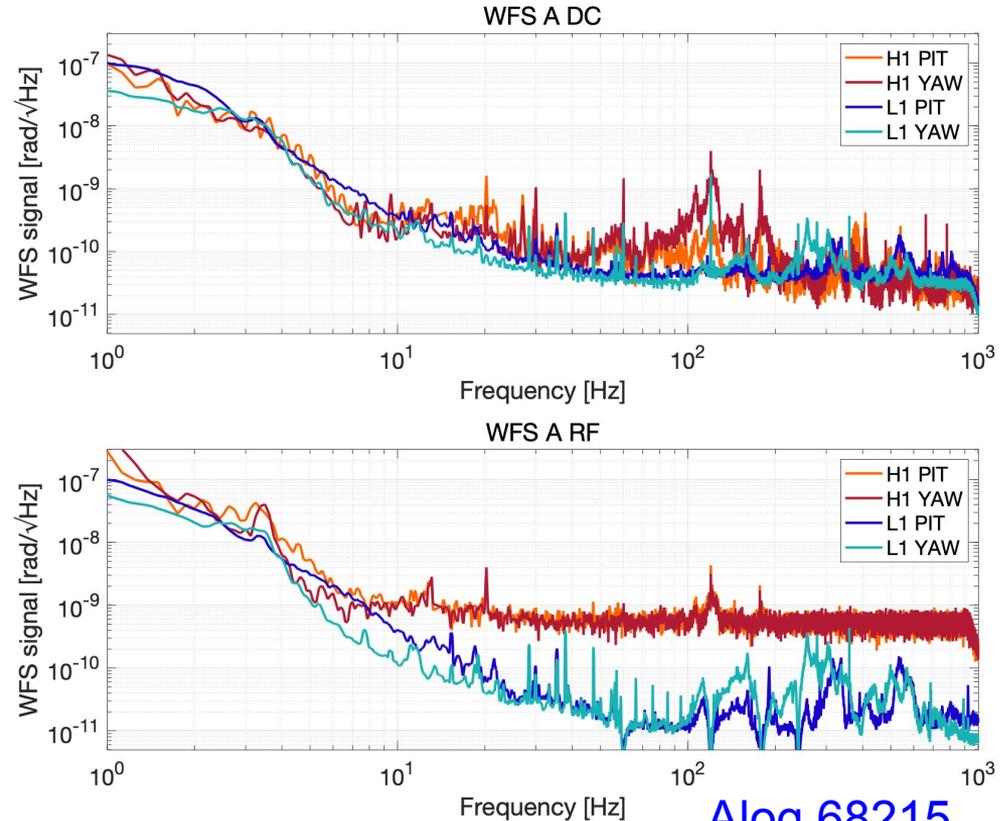
Example: Measuring Input Jitter

- IMC WFS are even better, and predict signal in DARM correctly!
- We add pit and yaw in quadrature since we can't distinguish



Example: Measuring Input Jitter H1 vs L1

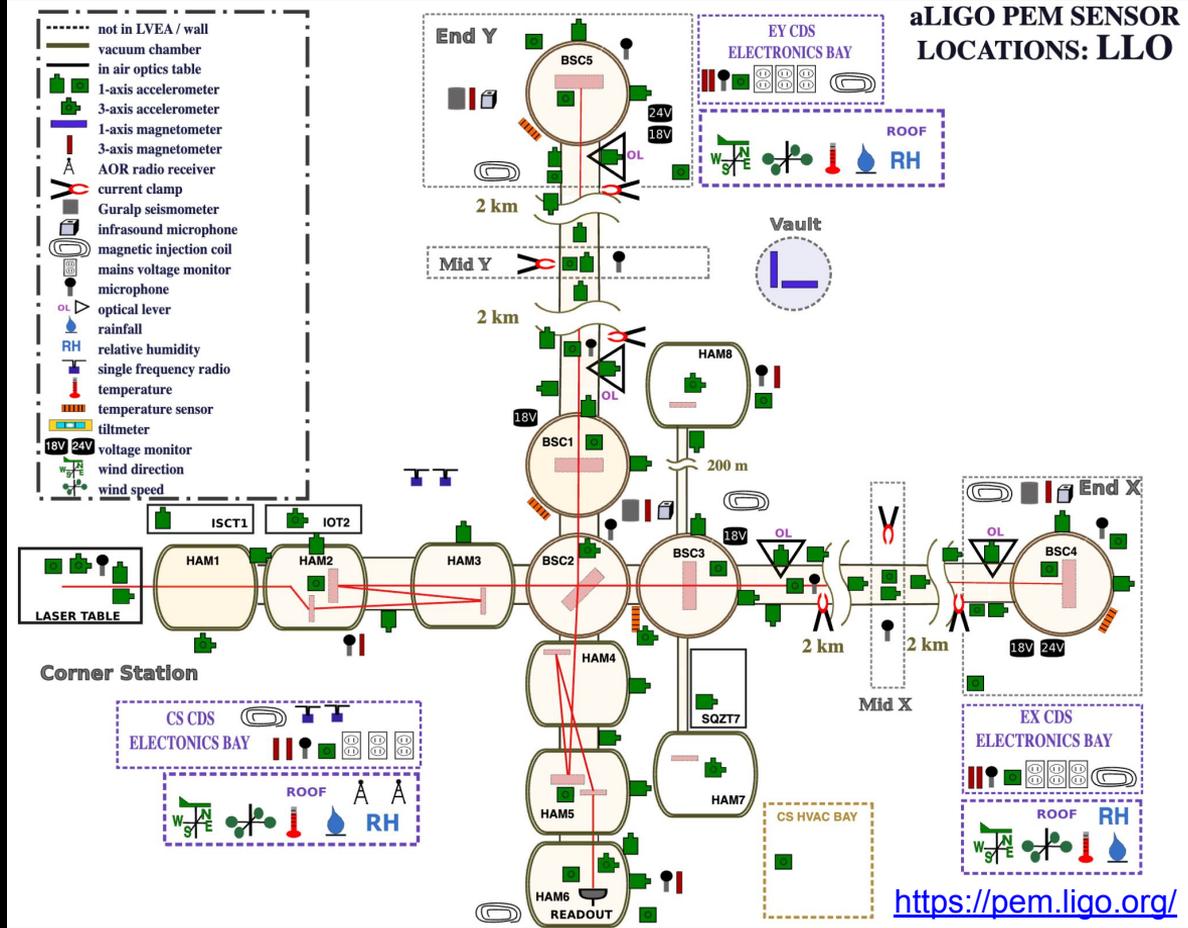
- H1 and L1 have similar coupling but H1 has a bit more ambient noise
- H1 and L1 have different best sensors!
 - H1: IMC WFS A DC
 - L1: IMC WFS A RF
- This coupling is subtracted in CALIB_STRAIN_CLEAN
- For O5 installing JAC (jitter attenuation cavity) to reduce by ~factor of 10



[Alog 68215](#)

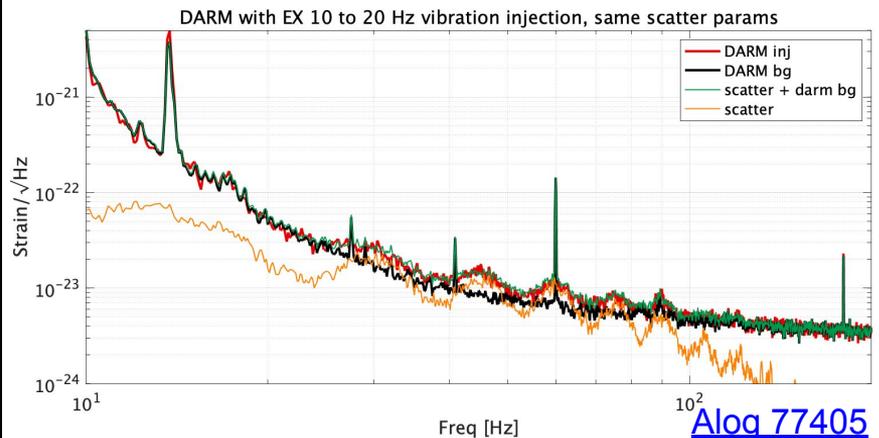
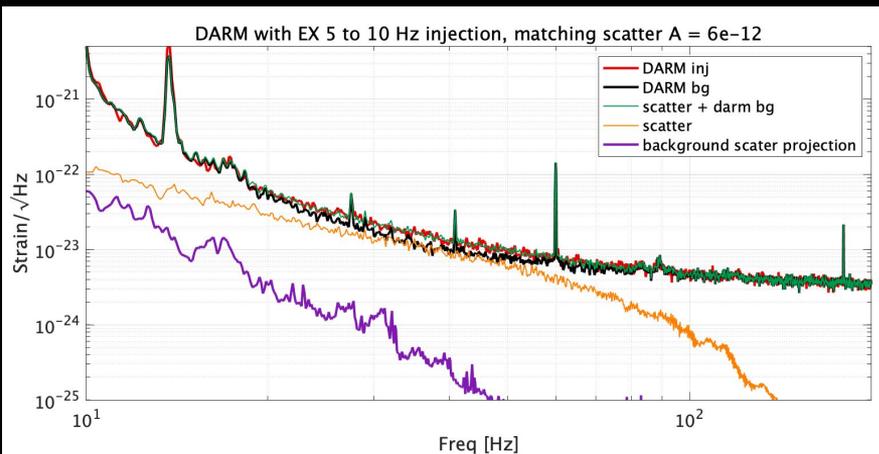
Ambient sources (PEM = physical environmental monitoring)

- Want **good coverage**: any noise source should make a larger signal in a sensor rather than DARM!
- Protection for data quality and vetoes
- Various measurements can point to noise sources and prioritize noise investigations



Upconverted noise example

- We can also model upconverted noise just fine as long as we have a physical model
- We can infer other parameters of the coupling (eg amount of light needed)



[Alog 77405](#)

Current schedule (L1, but H1 similar)

2025		2026								
Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sept
CY25Q4		CY26Q1			CY26Q2			CY26Q3		
PO4V1		(Post O4 Vent 1) - Duration TBD								
						Comm LLO	Comm - both			
Commissioning & PEM post Nov 18 ~2 weeks	BHD: Deinstall & HAM5/6 Septum Swap	BHD phase A [end of work ~start/mid April]								
TMDS X & Y (?) end	Laser interlock box upgrades	CHETA viewports & In-air install[mid Jan-mid Feb]		VMD's for ITMS	JAC/realign ISC table [~mid April - mid May] (during crnr pump down)					
	PLMP: Road repair and HVAC conversion (end stations)	BBSS with qOSEM & 2xCRS [end of work ~start/mid April] Cage Baffles on AR side of ITMs and stiffening brackets on ITMS								
	SEI upgrades L4C's, CPS, all BRS's and spring damper work (HAM 3 & 6)				ITM optic cleaning [at closeout of crnr vent]					
	CDS/EE prep work & upgrades (see list to left)				End station work (ISI, Baffles, optic cleaning) *X&Y Fix broken SEI sensors (requires dome removals) [done by early May]					
	Vent prep (test stands, platforms, cleanrooms, moving electronics, racks, etc)				SEI upgrades & spring damper work ? (HAM2, HAM4)					
		X end power outage work (~3 days work total)			Platform moves					
	Vacuum prep and upgrade tasks (see list to the left)									

Main items:
 BBS
 BHD ph.A
 CHETA
 JAC

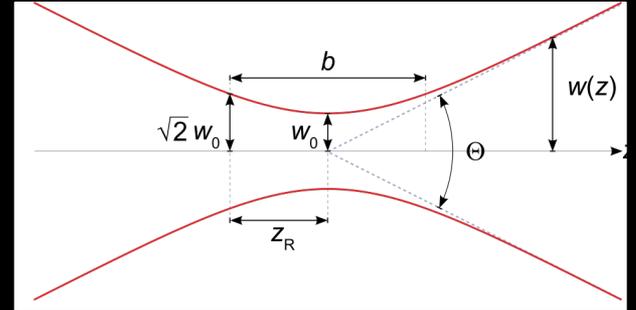
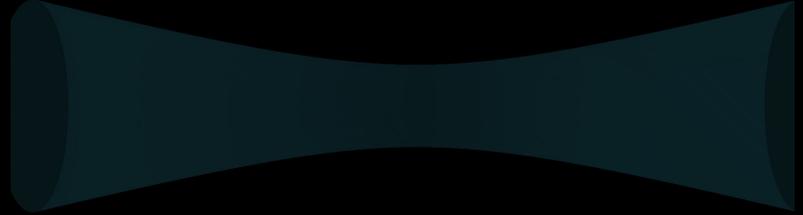
Nikhil from here on

Gaussian Beam

Exact solutions to EM wave equation under paraxial approximation

Lowest-order, minimum-divergence solutions supported by stable optical resonators

Natural eigenmodes of paraxial propagation and stable optical cavities.

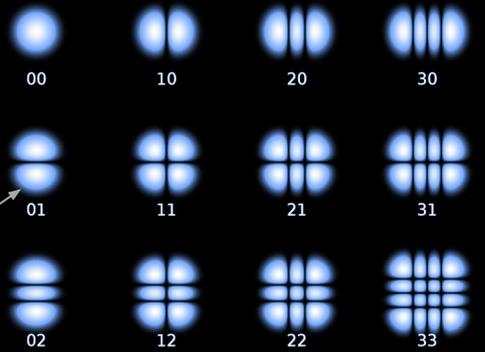


$$U(x, y, z, t) = U_0 \frac{w_0}{w(z)} \exp(-i\omega t) \exp\left[-\frac{x^2 + y^2}{w^2(z)}\right] \exp\left[-i\left(kz + \frac{k(x^2 + y^2)}{2R(z)} - \psi(z)\right)\right]$$

Laser Beam Quality

Paraxial approximation of laser beam model

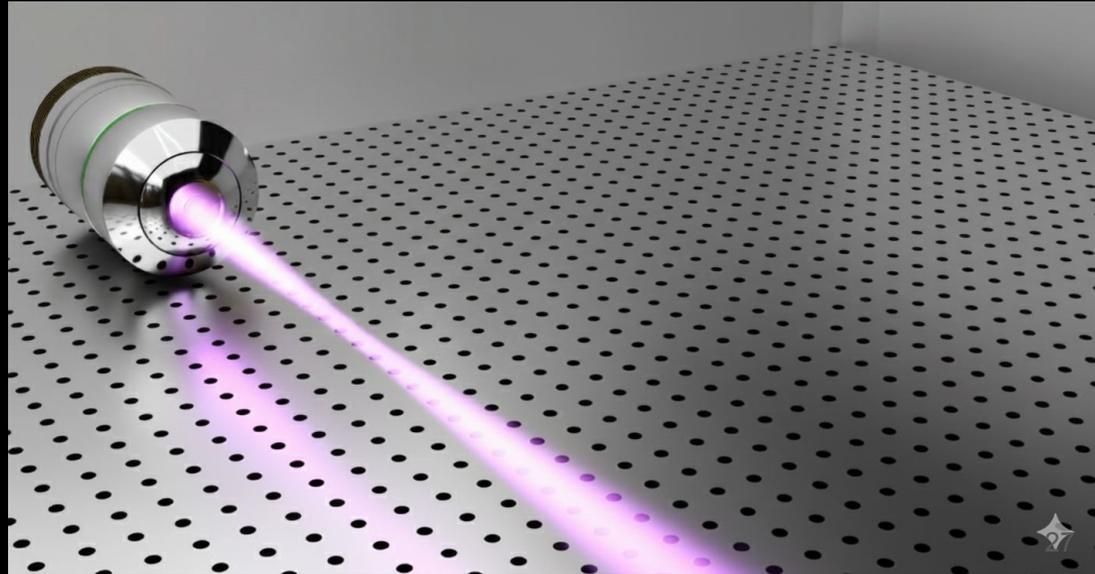
$$U(\vec{r}, t) = U_0(t) \exp(2\pi i \nu(t) t) \sum_{l, m \geq 0} c_{lm}(t) \Phi_{lm}(\vec{r})$$



Complex amplitudes of Hermite-Gaussian modes
TEM_{lm}

Fluctuations can occur in

- Power
- Frequency
- Beam quality
 - Spatial beam geometry
 - Beam pointing
 - Mode-matching
 - Astigmatism
 - Ellipticity



Relative Power Noise / Relative Intensity Noise

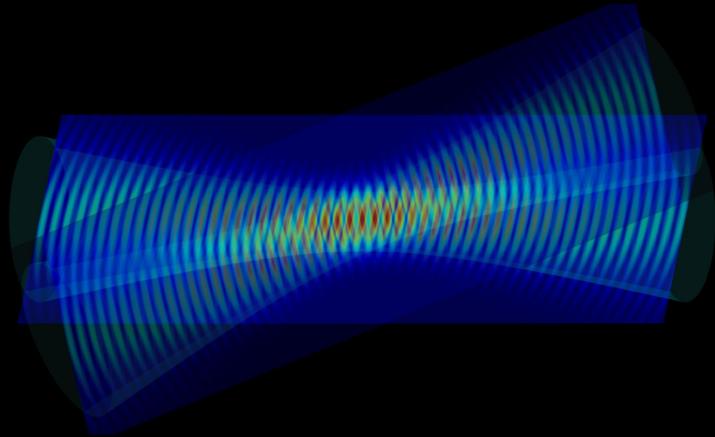
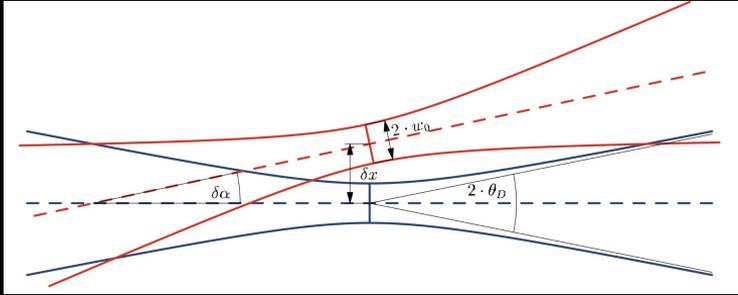
$$\frac{P(t)}{P_0} = \frac{|U_0(t)|^2}{\overline{|U_0(t)|^2}} \quad , \quad \overline{|U_0(t)|^2} = \frac{1}{T} \int_T dt |U_0(t)|^2$$

Beam Quality

Measured in terms of relative power in the fundamental TEM00 Mode

$$\frac{P_{\text{fund}}}{P_{\text{tot}}} = \frac{|c_{00}|^2}{\sum_{l,m} |c_{lm}|^2} = |c_{00}|^2$$

Beam Pointing Fluctuation Errors



$$\epsilon(t) = \frac{\delta x}{w_0} + i \frac{\delta \alpha}{\theta_D}$$

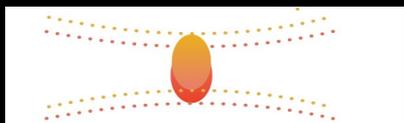
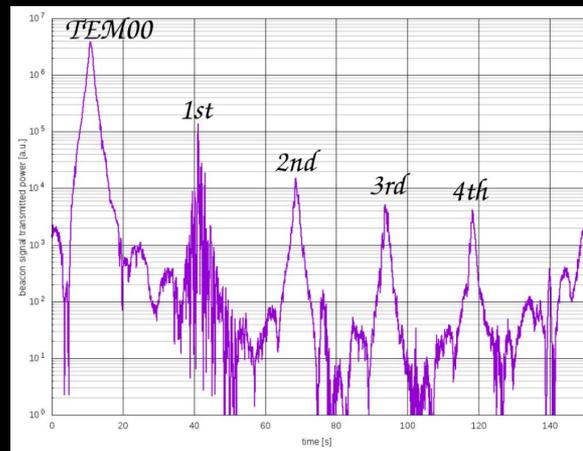
Fluctuation error, $\epsilon(t)$ of a shifted and tilted beam can be expanded Hermite-Gauss modes of the reference beam in terms of TEM₁₀ & TEM₀₁ relative amplitudes ($\epsilon \ll 1$ limit)

$$U(\epsilon_x, \epsilon_y) \approx \phi_{00} + \epsilon_x \phi_{10} + \epsilon_y \phi_{01}$$

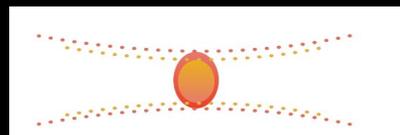
where

$$\epsilon_x(t) \approx \frac{C_{10}}{C_{00}}, \quad \epsilon_y(t) \approx \frac{C_{01}}{C_{00}}$$

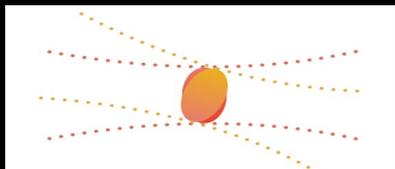
Detchar Example: Laser Beam Coupling to Cavity Eigen Modes



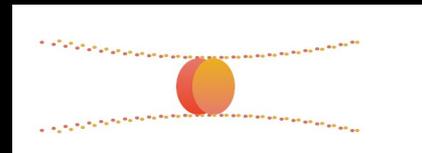
In phase coupling to 1st Order
(Beam Displacement)



In phase coupling to 2nd Order
(Waist size mismatch)



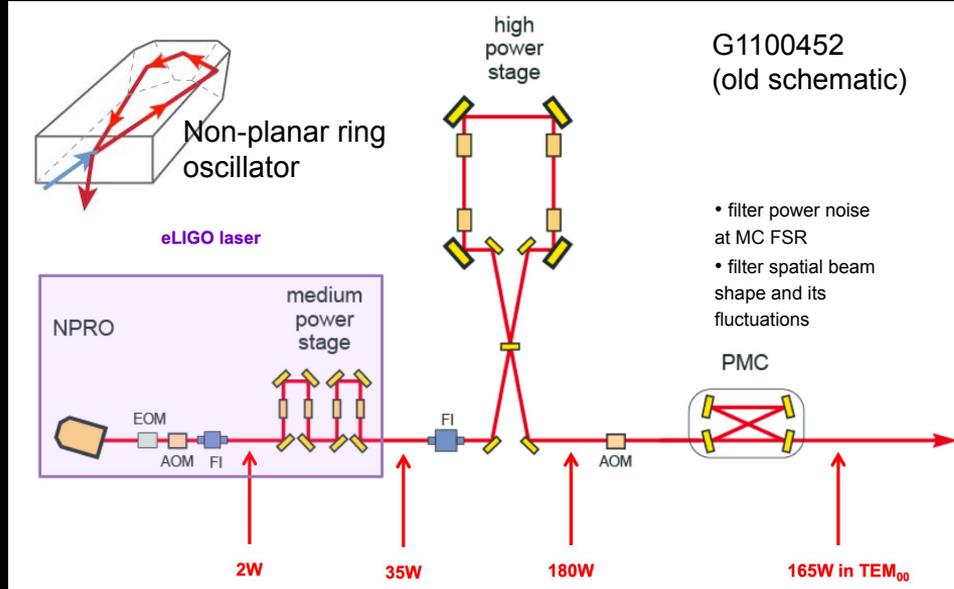
Quadrature phase coupling to 1st Order
(Beam Tilt)



Quadrature Phase coupling to 2nd Order
(Waist position mismatch)

LIGO Pre-Stabilized Laser

LIGO Pre-Stabilized Laser



Philosophy

Stabilize first at low power → amplify later → clean again

Requirements

Frequency stability

Power stability

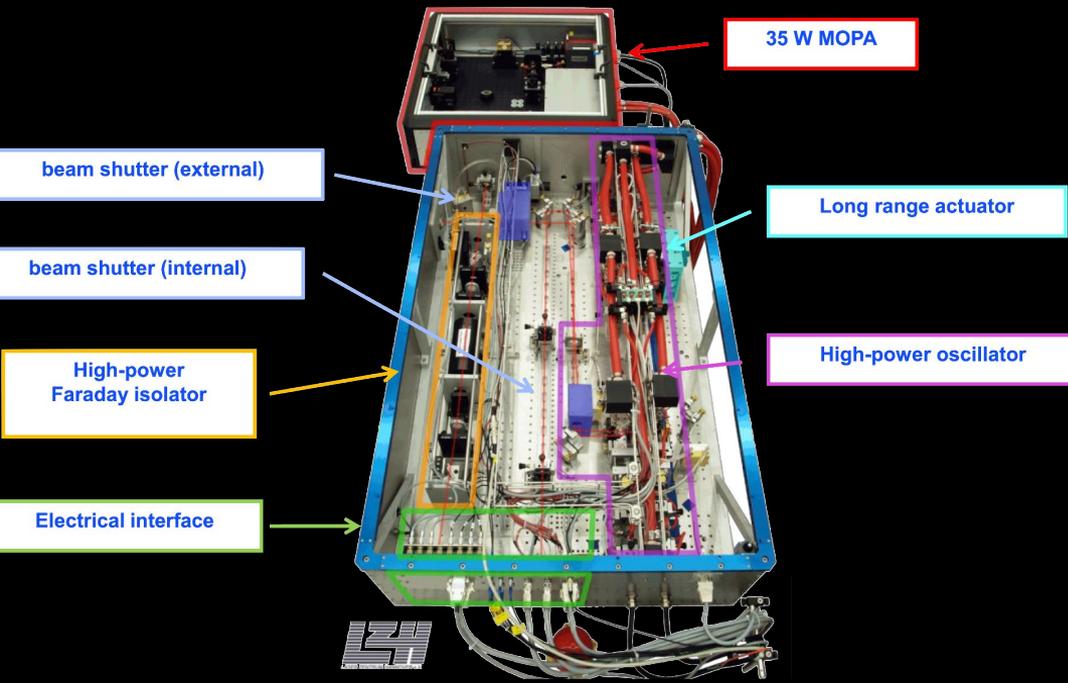
Pure spatial mode (TEM₀₀)

High Power
(200W in TEM₀₀, < 5W in higher non-TEM₀₀)

Reliable & controllable

5% power drift over 24hrs
100 kHz frequency drift over 100s

LIGO Pre-Stabilized Laser

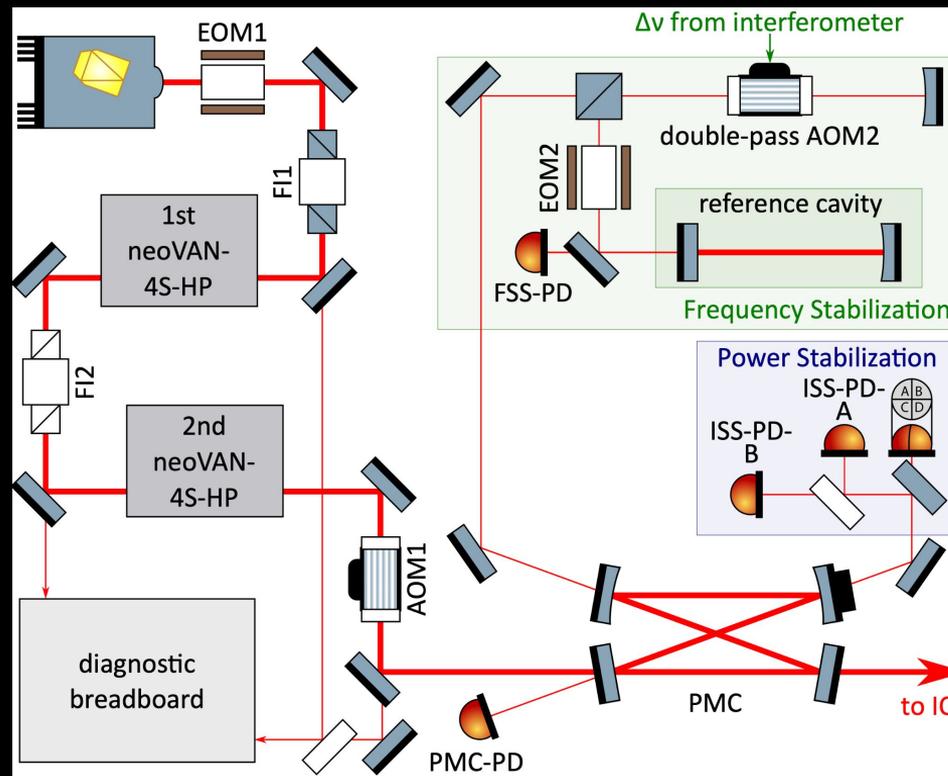
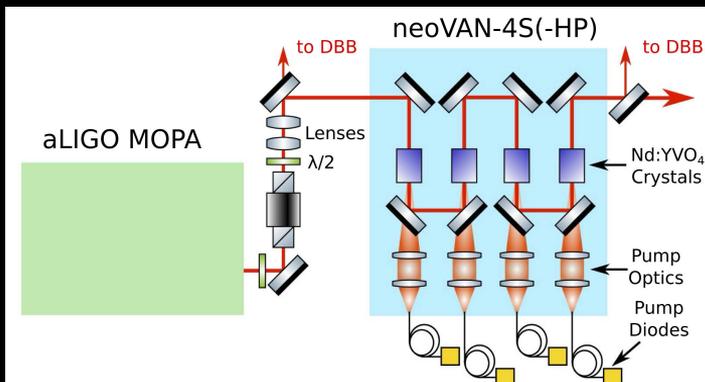


HPO requires strong water cooling, and cooling-driven vibrations creates beam pointing/size noise, which couples badly to the detector.

Can also suffer from cavity length noise, thermal noise etc.

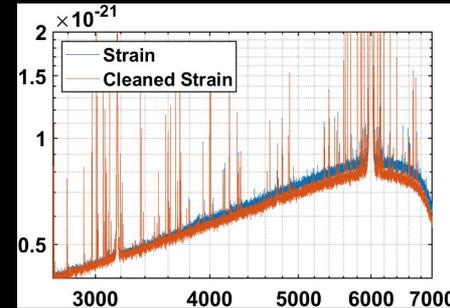
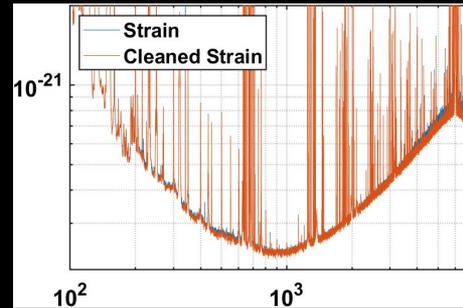
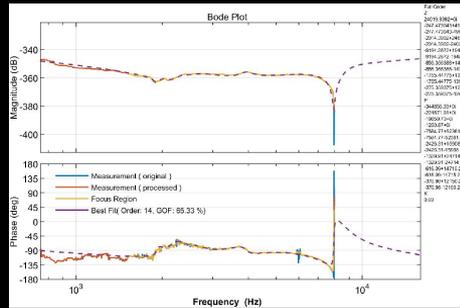
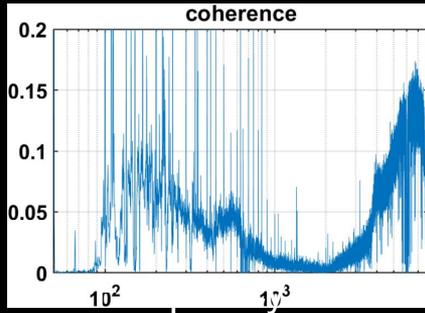
LIGO PSL O4 Latest Schematic

High power oscillator replaced with amplifier stage.



Output power : 140W

Detchar Example: Laser Amplitude Noise Subtraction



Step 1.
Measure
coherence
with strain

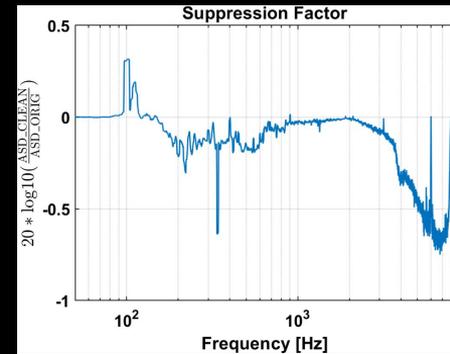
Identify
coupling

Step 2.
Measure transfer function
from witness to GW
strain channel

Do system identification.
Fit IIR/FIR filter

Step 3.
Do time domain
subtraction

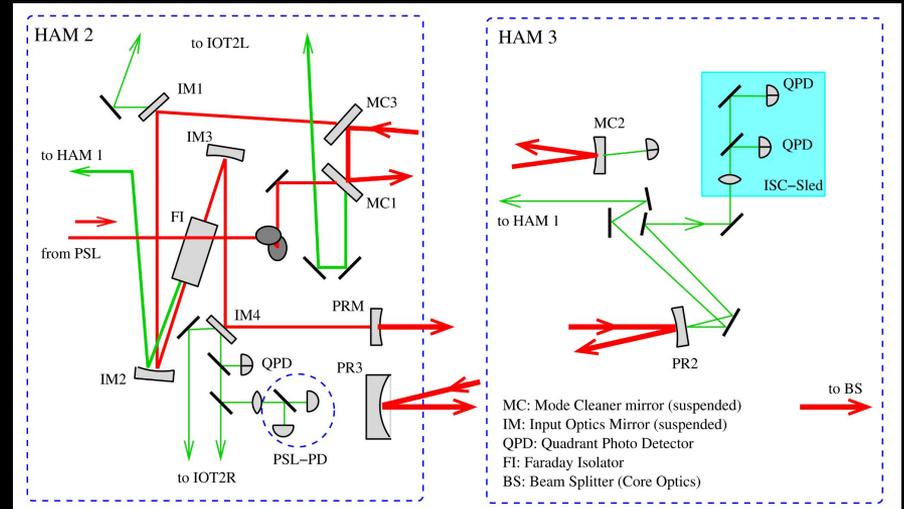
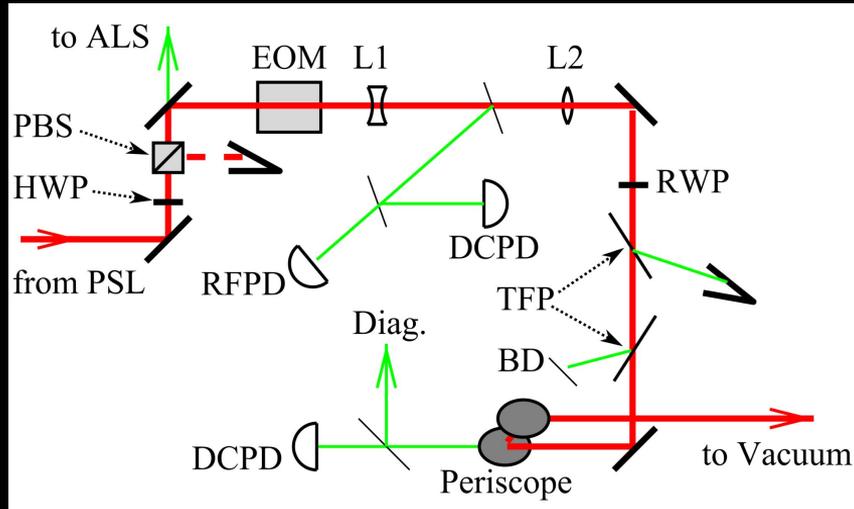
Check suppression/
residual coherence



Input Optics

Input Optics

Main task: Take the beam from PSL, prepare it and inject it to main interferometer.

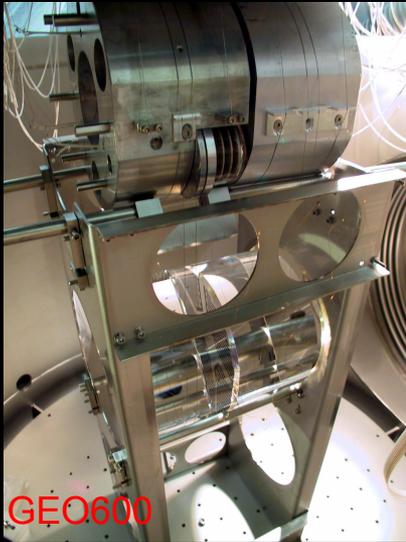


Outside vacuum, co-located with PSL

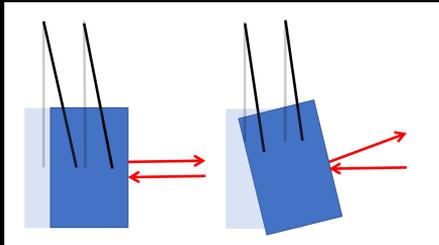
In vacuum, seismically isolated

Alignment Sensing & Control (ASC)

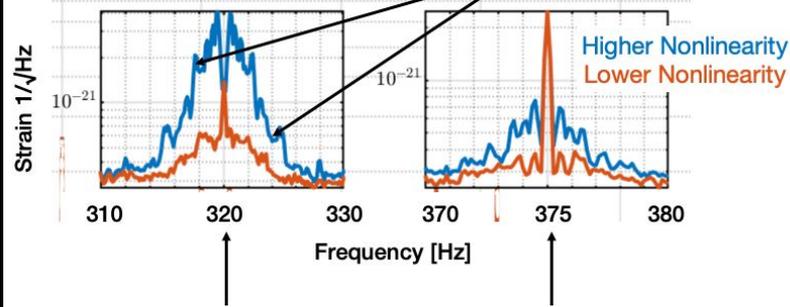
Misalignments affect strain sensitivity



- Angular Motion is imprinted in the strain signal in a broadband sense.
- Increases the number of transients -> false GW triggers
- Persistent sidebands also effect continuous wave searches

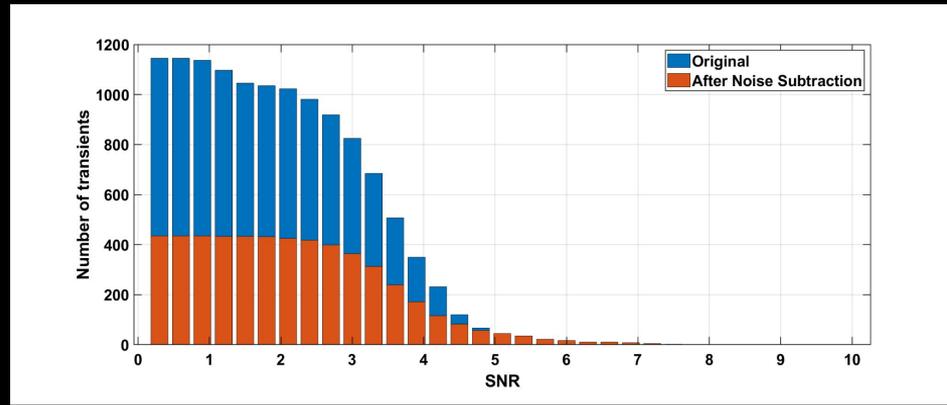
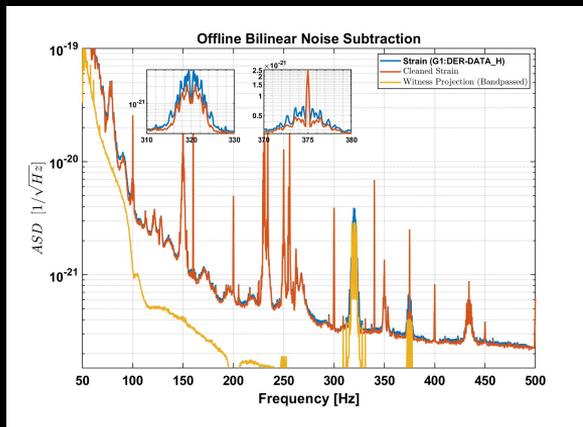
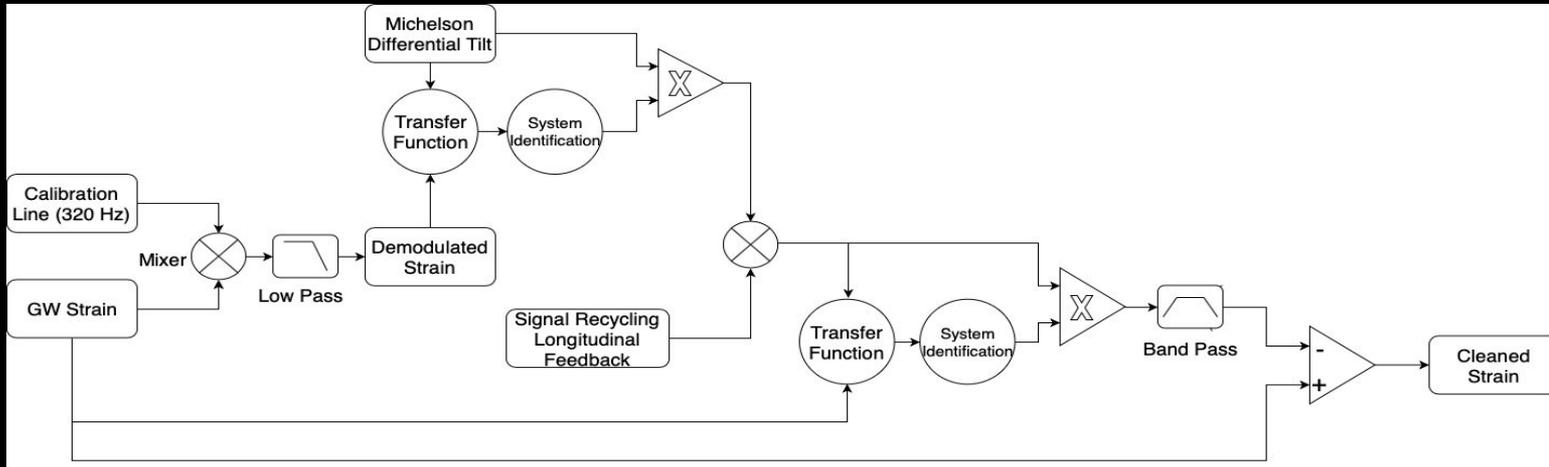


Bilinear Coupling: Injected narrowband frequency lines get modulated by low frequency alignment fluctuations leading to sidebands.

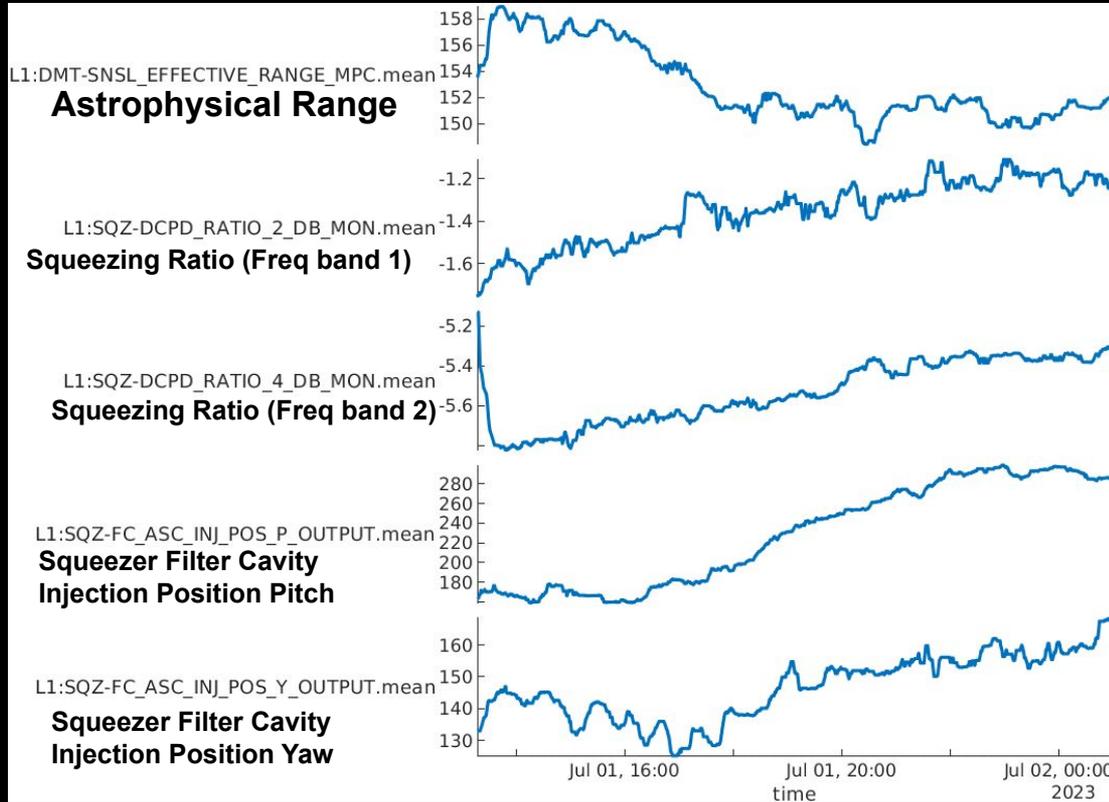


Single frequency calibration lines

DetChar Example: Removing Bilinear Coupling

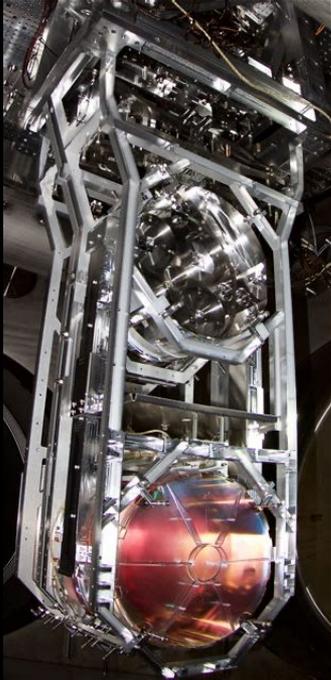


DetChar Example: Squeezer Filter Cavity Misalignment Correlates with Astrophysical Sensitivity Degradation

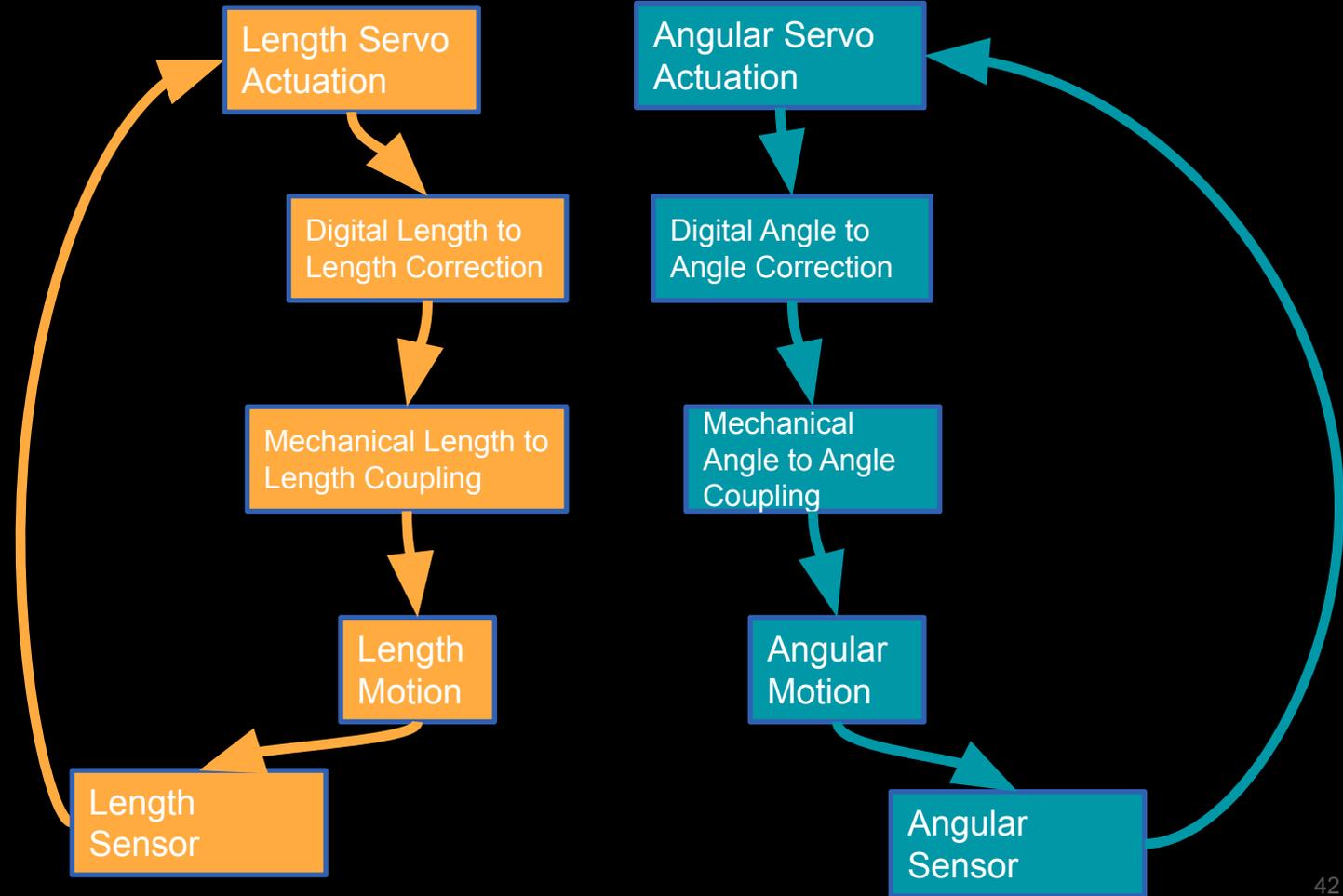


Ideal

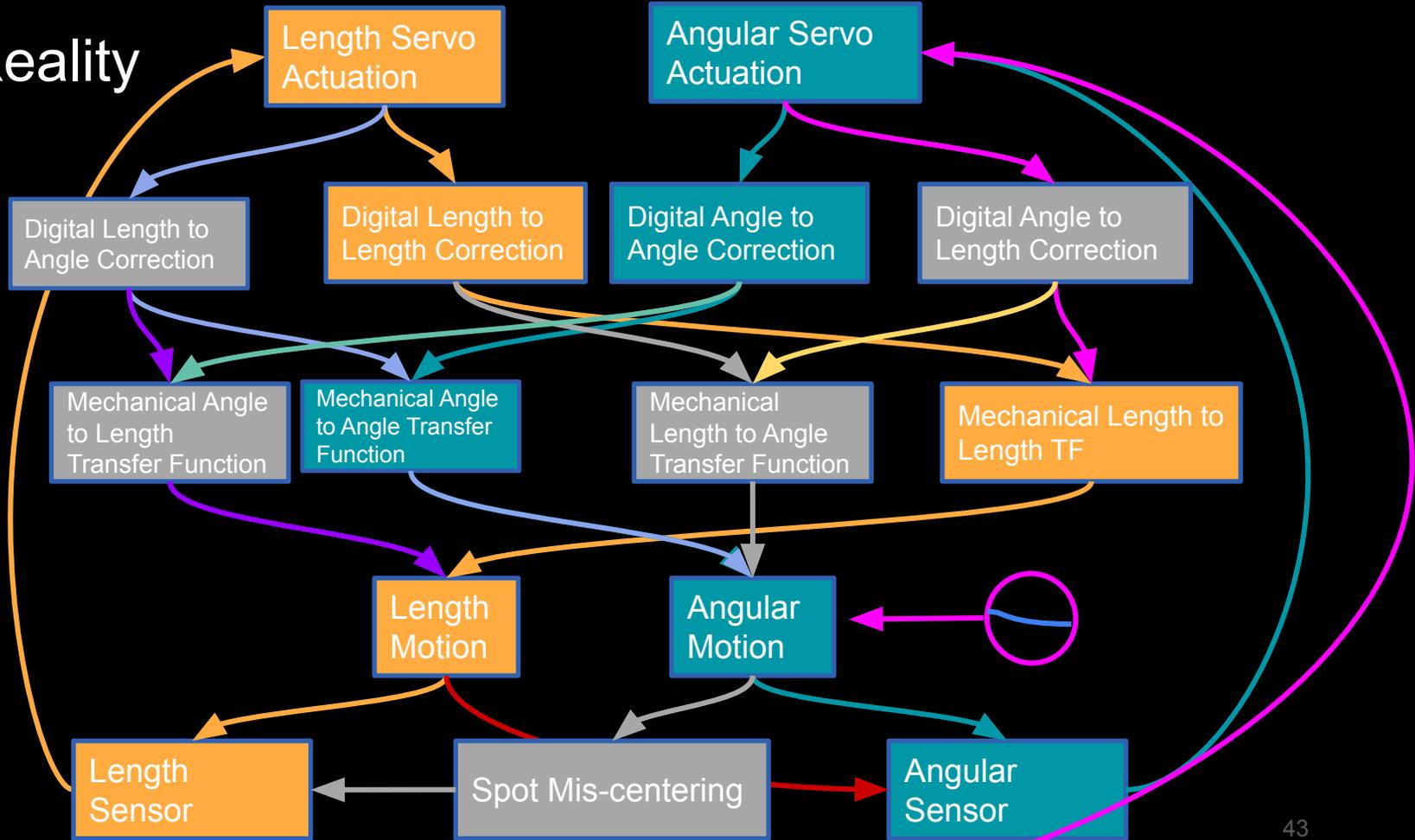
Controlling Suspended Optics



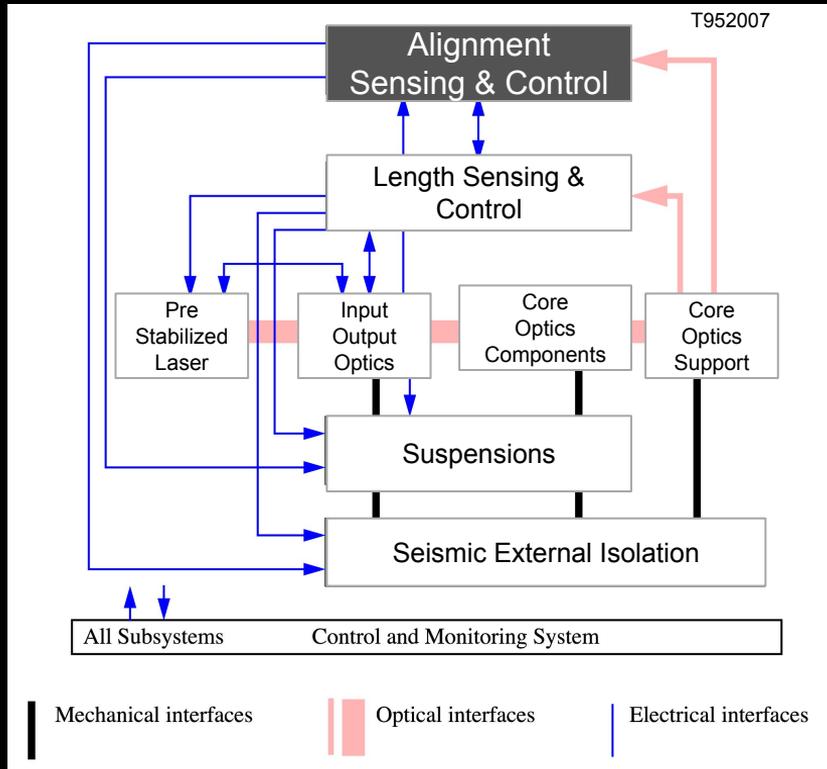
Advanced LIGO
40kg test mass



Reality



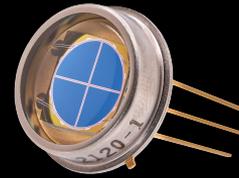
Alignment Sensing & Control (ASC)



Any hardware and/or algorithms used for

- Determination of initial interferometer optical axes
- Initial alignment of input-output optics and suspended core-optics
- Determination and control of beam position on the suspended core-optics

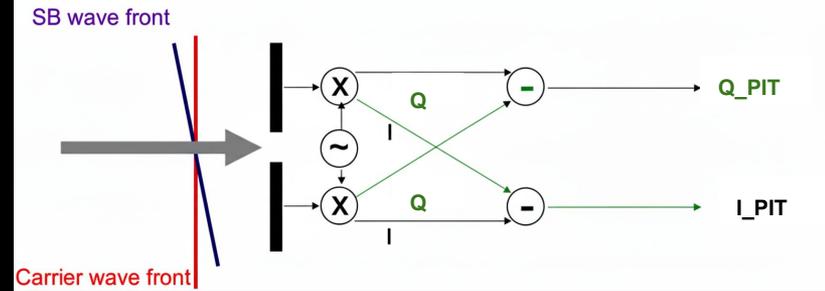
ASC Sensors : QPD & WFS



Quadrant Photodiode

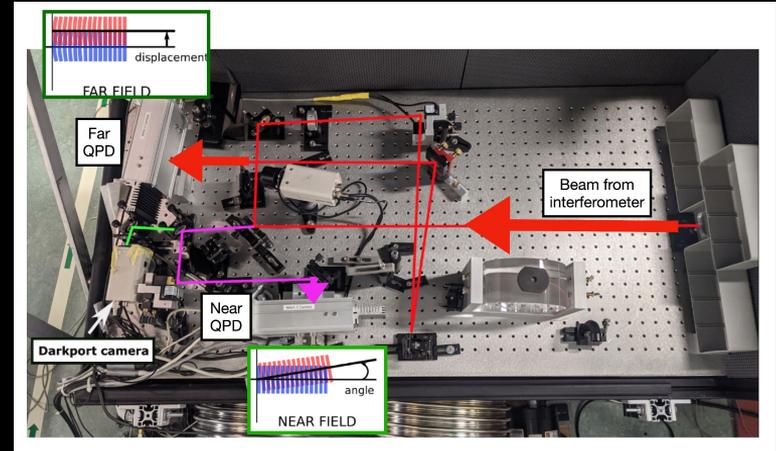
Gives info about the beam position of the QPD
(good for pointing/drift control)

Pitch = (top-bottom)/sum
Yaw = (left-right)/sum

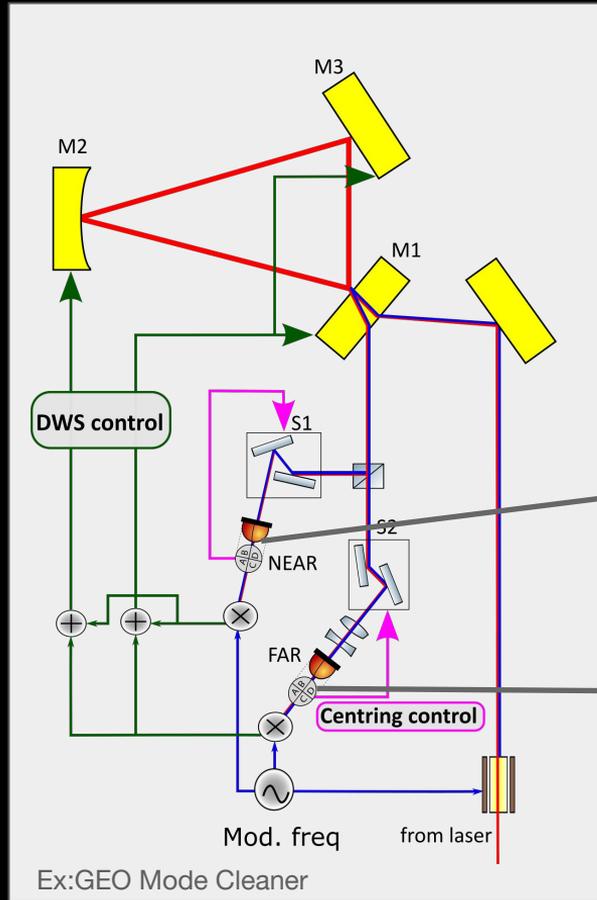


Wave Front Sensor

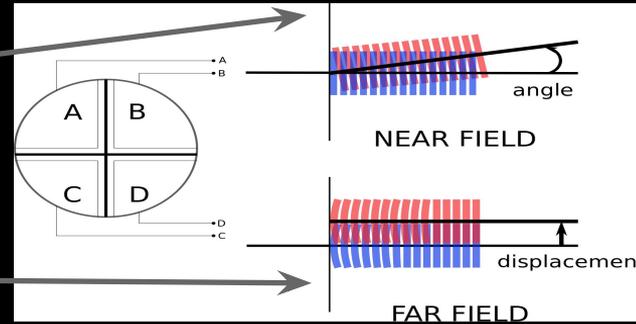
- Relative alignment info btw two laser fields at two frequencies (carrier & sideband)
- Each sensor head is a Radio Freq QPD
- Each quadrants get demodulated by Cos & Sin (I & Q)
- 8 initial signals combined to 4 (Pitch/Yaw, I/Q) per WFS



Differential Wavefront Sensing (DWS)



- Mark the incident field to a cavity with a reference frequency, which is promptly reflected
- Demodulate the "near" and "far" quadrant photodetector signals at the reference frequency



Relative Gouy phase between the near and far QPD is 90°

- DWS can sense four misalignments in total (horizontal, vertical) x (angle, displacement)

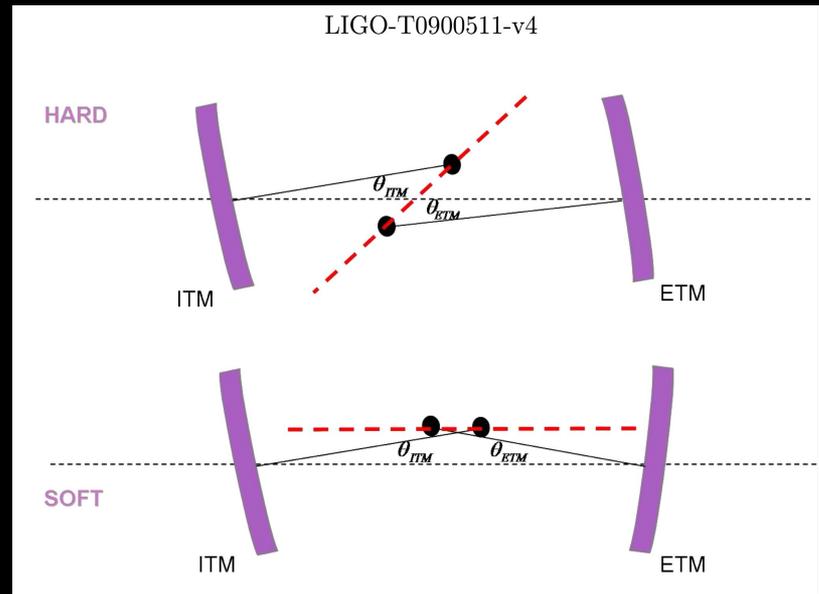
Hard and Soft Modes

- At high power, radiation pressure from the laser couples to the cavity mirrors
- Laser acts like a rotatory spring along pitch (yaw) axis

$$\vec{\tau}_{\text{opt}} = \begin{bmatrix} T_i \\ T_e \end{bmatrix} = \mathbf{K}_{\text{opt}} \begin{bmatrix} \theta_i \\ \theta_e \end{bmatrix}$$

$$\mathbf{S}^{-1} \begin{bmatrix} k_{\text{soft}} & 0 \\ 0 & k_{\text{hard}} \end{bmatrix} \mathbf{S} = \mathbf{K}_{\text{opt}}$$

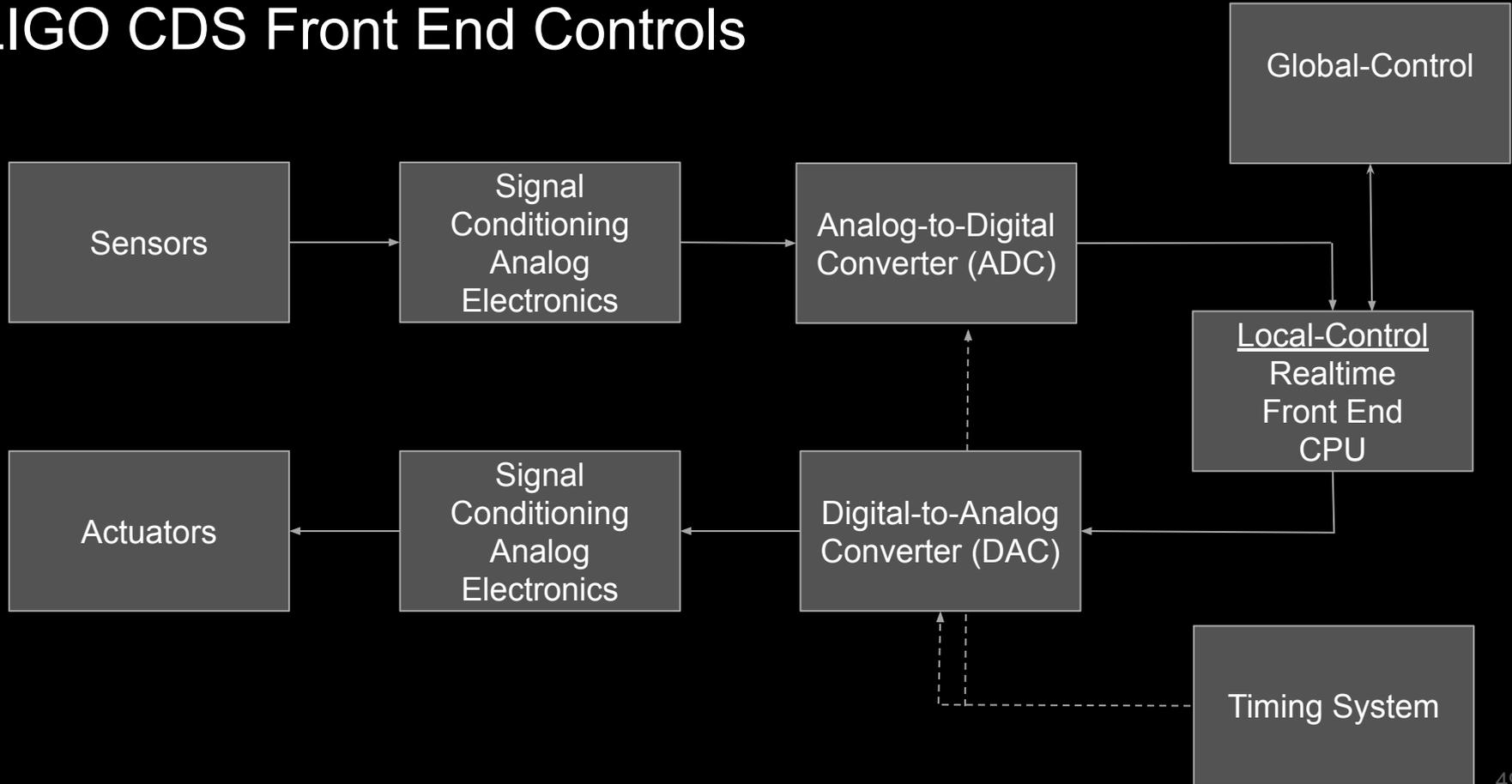
- Hard (soft) modes have higher (lower) frequency than individual suspensions



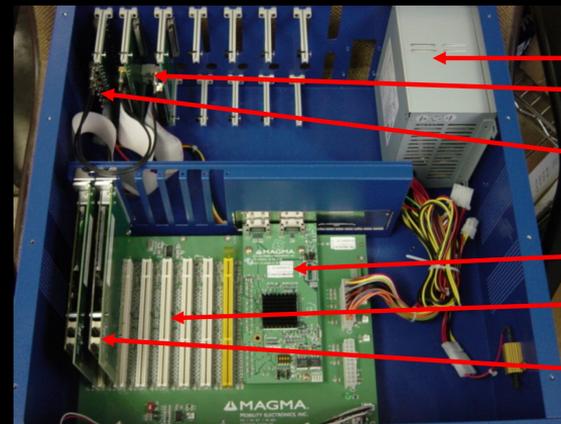
- Hard mode -> higher g-factor->higher sensitivity -> damped at higher bandwidth using ETMs
- Soft mode -> lower g-factor->higher sensitivity -> damped at lower bandwidth using ITMs

Controls & Data Systems (CDS)

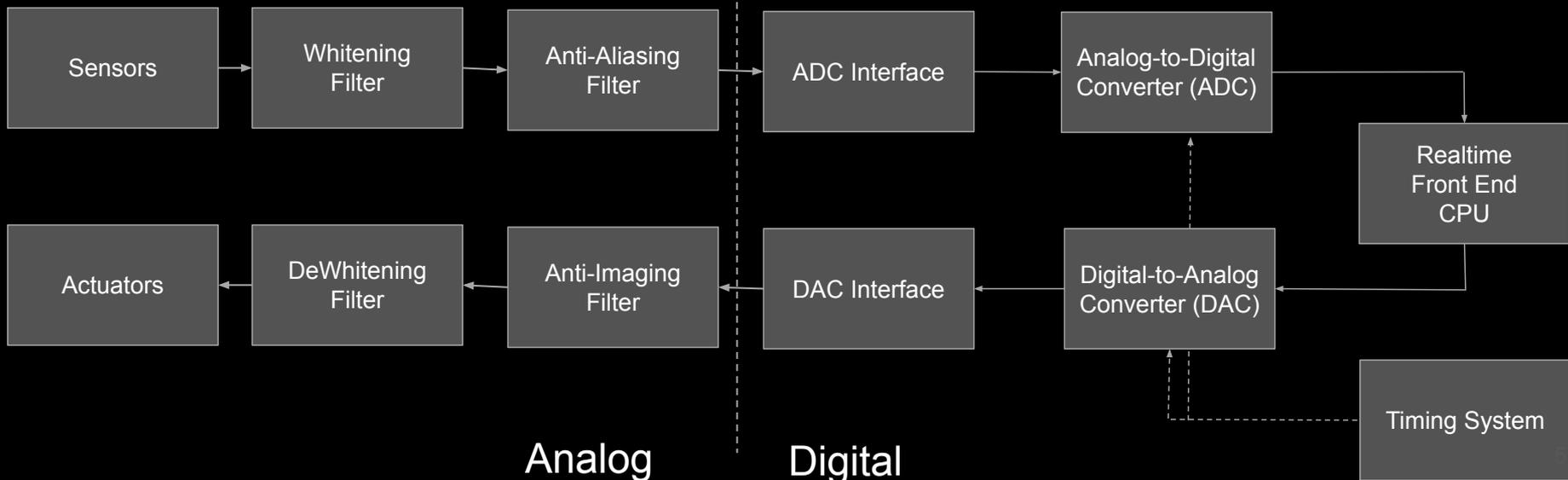
LIGO CDS Front End Controls



LIGO CDS Front End Controls

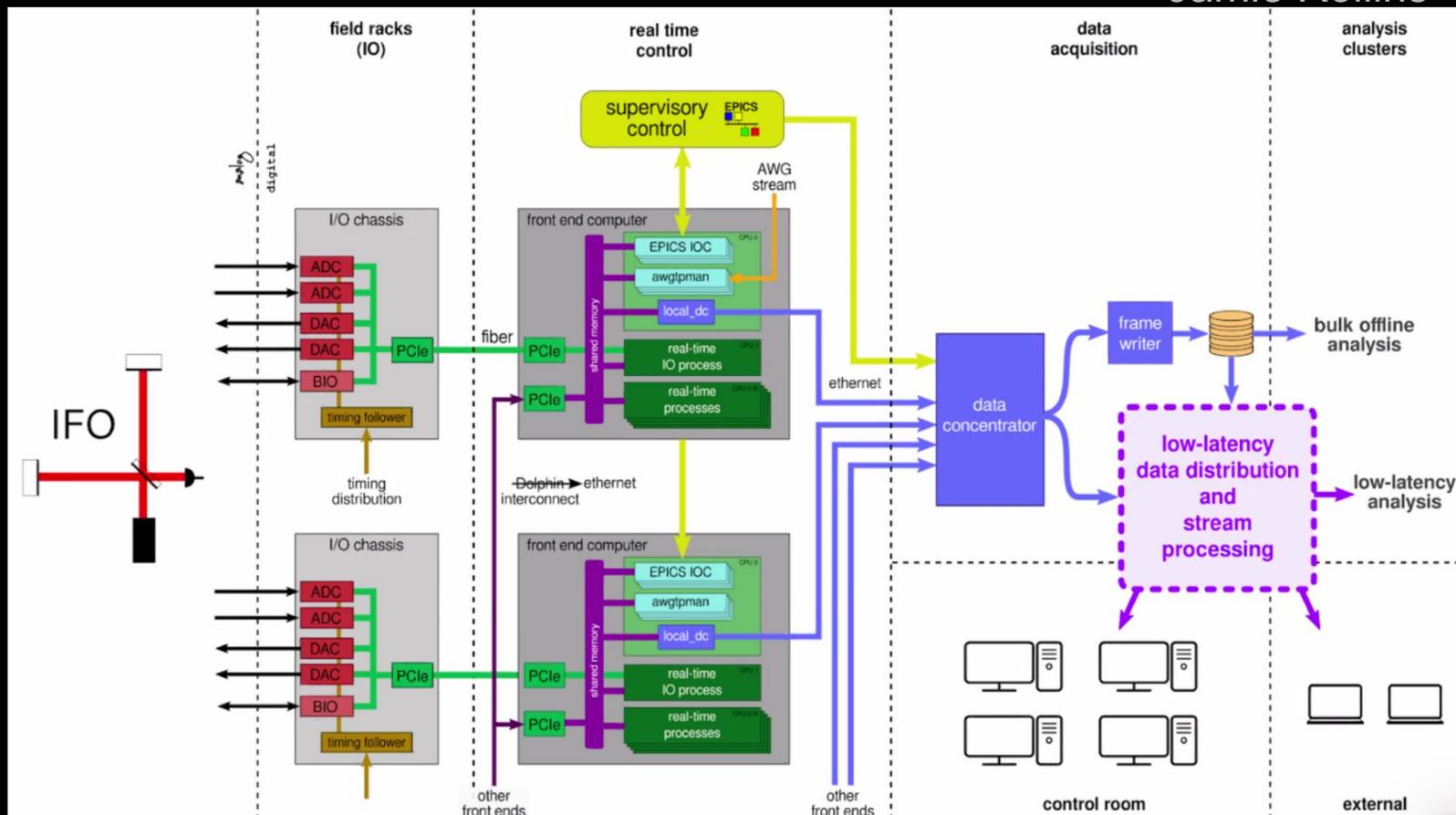


- Power Supply
- ADC/DAC Interface Board
- Timing Interface
- Fiber Uplink
- PCIX/PCIe Bus
- ADC & DACs

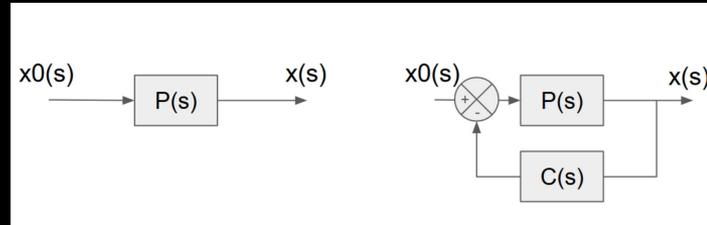
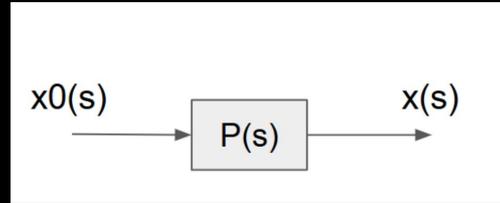


LIGO CDS Front End Controls

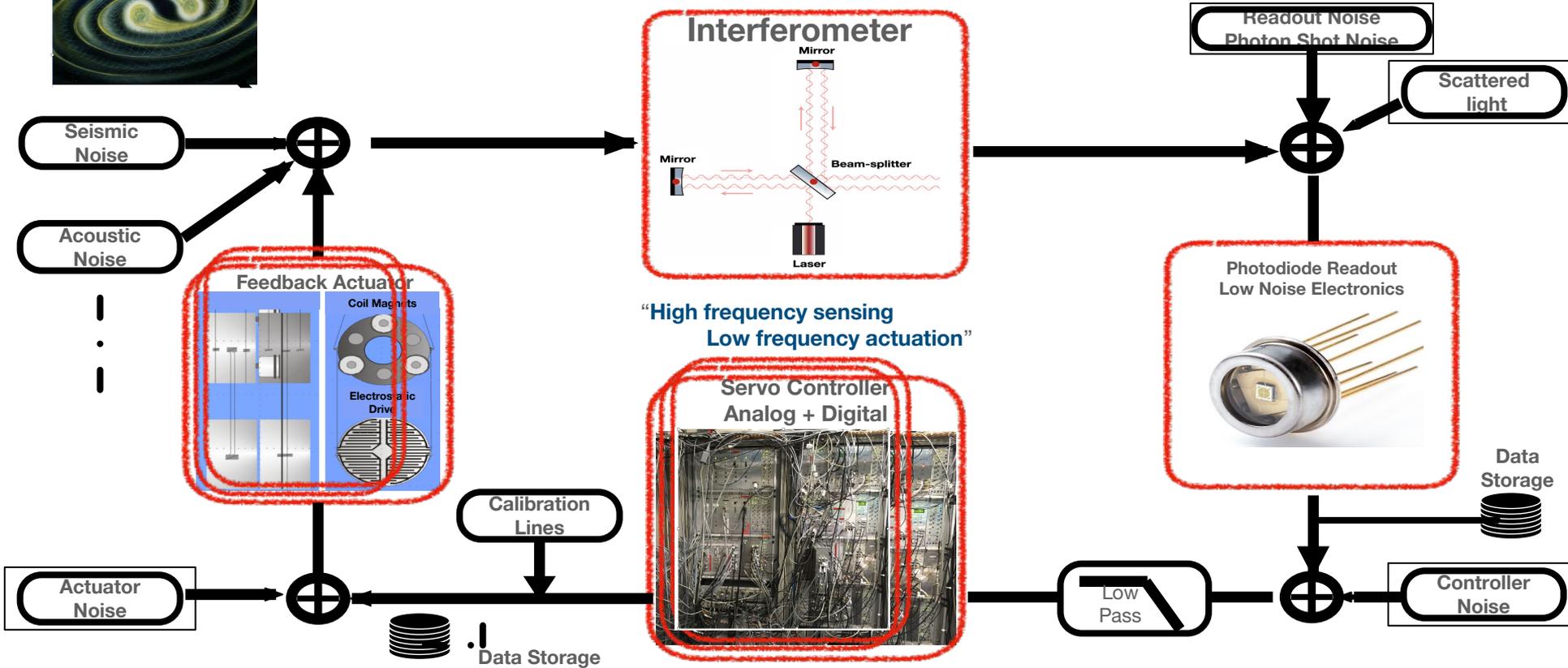
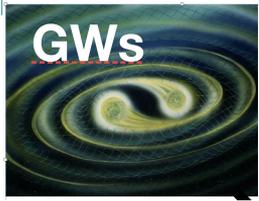
Jamie Rollins



Control Loops

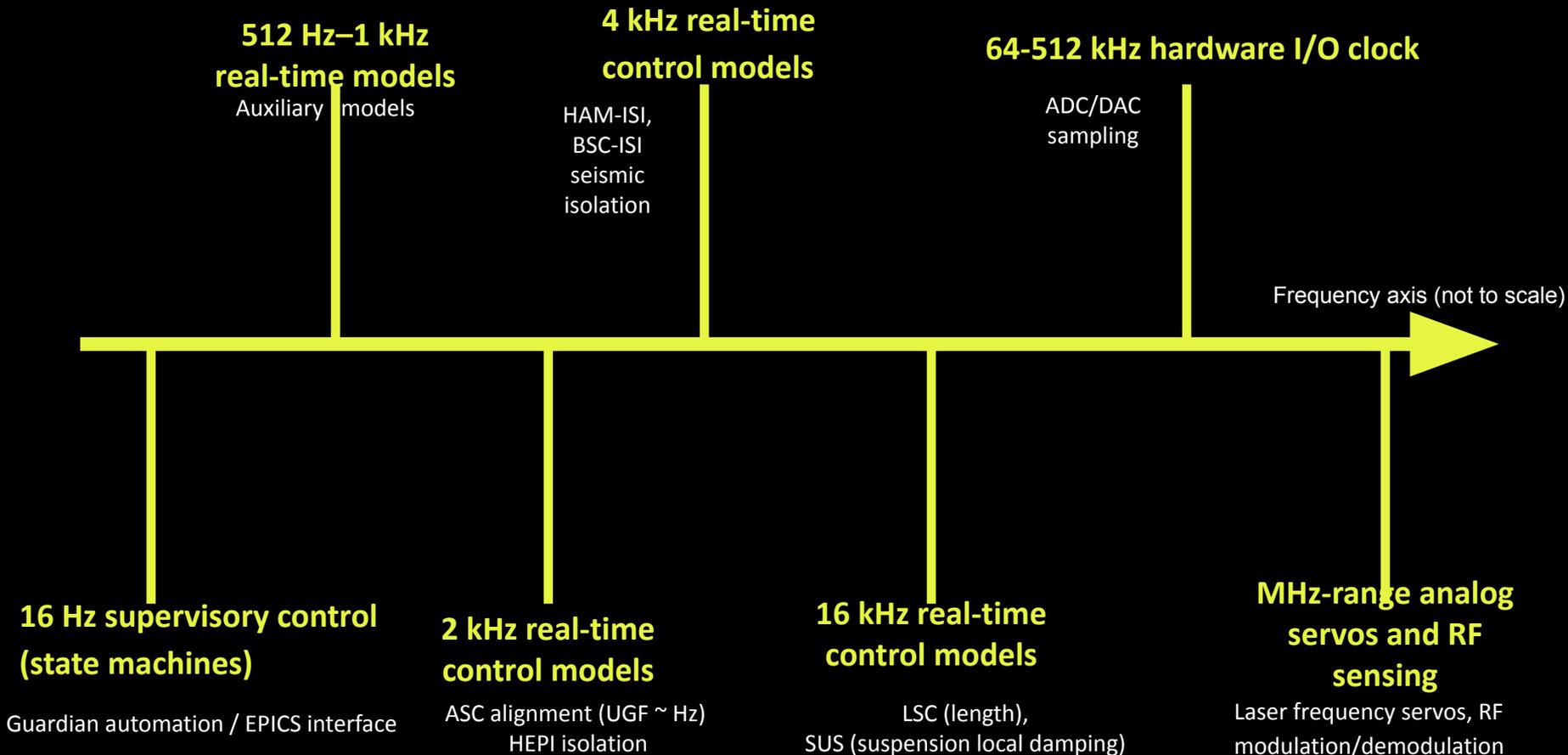


How a GW interferometer listens to GWs...

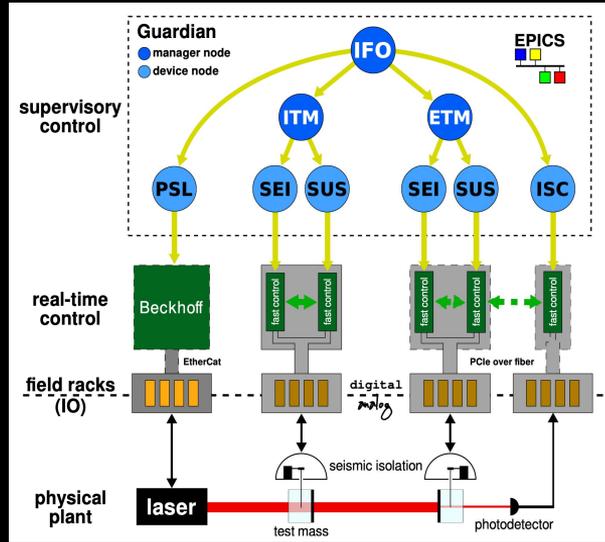


Control Frequency Hierarchy

Model rate = digital controller execution rate
UGF = closed-loop control bandwidth



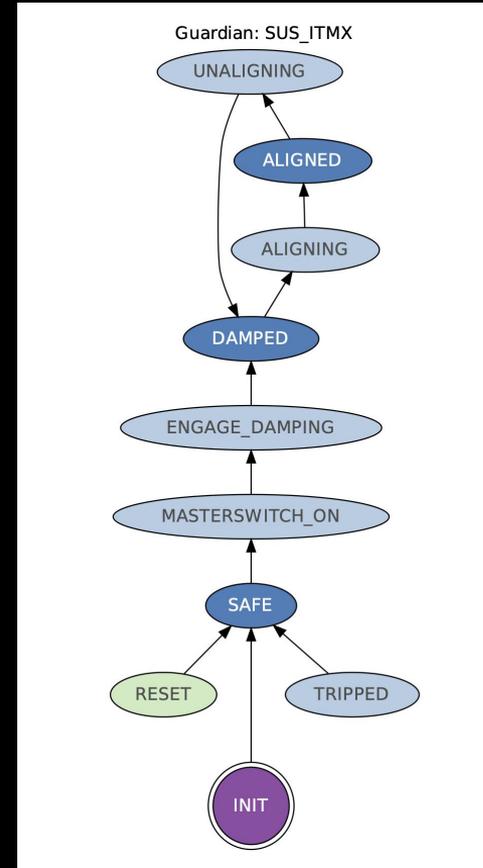
GUARDIAN: Hierarchical State Machine



ArXiv: 1604.01456v1

Manages the global state of the interferometer by coordinating subsystem states

Each node loads a directed state graph: states are executable code blocks; edges define allowed transitions.



Control Loop Bands in Advanced LIGO

MHz range (analog):

PSL and IMC frequency-stabilization loops; PDH servos.

Unity-gain bandwidth roughly 0.8–1 MHz for laser-frequency loops.

RF phase modulation and demodulation at approximately 10–50 MHz.

64 kHz hardware clock:

ADC and DAC timing; front-end I/O processors.

16 kHz fast digital models:

LSC : global longitudinal control (DARM, CARM, etc.). LSC model runs at 16 kHz.

Core suspension (SUS) models : QUAD suspension local damping and actuator interface.

DARM servo unity-gain typically 40–100 Hz.

4 kHz band:

HAM-ISI and BSC-ISI in-vacuum seismic-isolation controllers. Sensor inputs are digitized at 64 kHz then decimated to 4 kHz.

2 kHz band:

HEPI external seismic-isolation platforms.

Many ASC and angular-control front-end models run at 2 kHz or 4 kHz; typical alignment loop unity-gain around 1–3 Hz.

512 Hz–1 kHz band:

Various other fast digital models (thermal-compensation systems, auxiliary controls), depending on site and configuration.

16 Hz slow control:

Guardian automation state machines for lock acquisition and recovery.

EPICS “slow” operator-monitoring channels.

Gravitational-Wave Observatory Status

Please select a date from the calendar above to see archived or current status.

Information is available for dates after November 30, 2016. The Advanced LIGO and Virgo detectors have begun the third part of the fourth observing run, known as O4c, as of January 28, 2024. The entry of the KAGRA detector into O4c has been postponed in order to continue detector commissioning activities and further increase the sensitivity of the detector. All detectors are planned to rejoin O4 by the end of the run. Summaries of the [current observing run](#) and previous observing runs are in the menu above. For overviews of LIGO, Virgo, and KAGRA observing runs, see the [arXiv:1304.0670](#).

- [Today's Summary Page](#)
- [Current Status \(GWSTAT\)](#)
- [LIGO/Virgo Alerts \(GraceDB\)](#)
- [Hanford alog](#) – [Livingston alog](#) – [Virgo logbook](#) – [KAGRA klog](#)
- [LIGO Laboratory](#) – [Virgo](#) – [KAGRA Observatory](#) – [GEO600](#)



LIGO Hanford



LIGO Livingston



Virgo



KAGRA



GEO600

https://gwosc.org/detector_status/day/20251001/environment/ground_motion/

Environment : Ground motion

These plots display the ground motion at the LIGO Livingston and LIGO Hanford Observatories as measured by Streckeisen STS-2 sensors. Each plot shows the root-mean-square ground motion in a different frequency band, which capture independent ground motion behavior.

