

# Linear systems for gravitational-wave detectors

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# Section 1

## Preliminaries

# Bilateral Laplace transform

Given a time-domain function  $g(t)$ , its Laplace transform  $\tilde{g}(s)$  is

$$\tilde{g}(s) = \int_{-\infty}^{+\infty} dt e^{-st} g(t)$$

The variable  $s$  is a *complex angular frequency*. We'll also write the Laplace transform as an operator  $g(t) \xrightarrow{\mathcal{L}} \tilde{g}(s)$ .

When  $s = i\Omega$ , this is also a Fourier transform:  $g(t) \xrightarrow{\mathcal{F}} \tilde{g}(\Omega)$ .

# Some Laplace transform properties

*Time shifts become phase delays:  $g(t - \tau) \xrightarrow{\mathcal{L}} e^{-s\tau} \tilde{g}(s)$*

*Time derivatives become frequency rescalings:  $\dot{g}(t) \xrightarrow{\mathcal{L}} s \tilde{g}(s)$*

In particular:

- $\dot{x}(t) \xrightarrow{\mathcal{L}} s \tilde{x}(s) = -i\Omega \tilde{x}(\Omega)$
- $\ddot{x}(t) \xrightarrow{\mathcal{L}} s^2 \tilde{x}(s) = -\Omega^2 \tilde{x}(\Omega)$

# Solving equations in the Laplace domain

Damped harmonic oscillator (time domain):

$$m\ddot{x}(t) = -m\Omega_0^2 x(t) - m\Gamma\dot{x}(t) + F(t)$$

Damped harmonic oscillator (Laplace domain):

$$ms^2\tilde{x}(s) = -m\Omega_0^2\tilde{x}(s) - m\Gamma s\tilde{x}(s) + \tilde{F}(s)$$

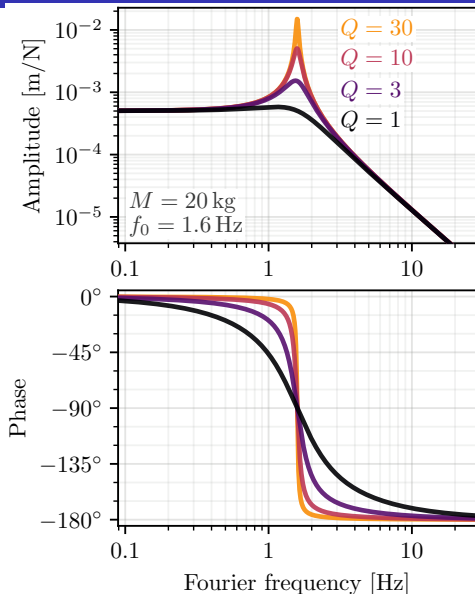
Allows us to write the system's *frequency response* or *transfer function*:

$$\frac{\tilde{x}(s)}{\tilde{F}(s)} = \frac{1/m}{\Omega_0^2 + s^2 + \Gamma s}$$

# Frequency response of the damped harmonic oscillator

Taking  $s = i\Omega$  and defining  $Q = \Omega_0/\Gamma$ :

$$\frac{\tilde{x}(\Omega)}{\tilde{F}(\Omega)} = \frac{1/m}{\Omega_0^2 - \Omega^2 + i\Omega_0\Omega/Q}.$$



# Zero–pole–gain representation

If  $\tilde{g}(s)$  is rational, it can be factorised:

$$\tilde{g}(s) = k \frac{(s - z_0)(s - z_1)(s - z_2) \cdots}{(s - p_0)(s - p_1)(s - p_2) \cdots}$$

where  $\{z_i\}$  are the zeros,  $\{p_i\}$  the poles, and  $k$  the gain.

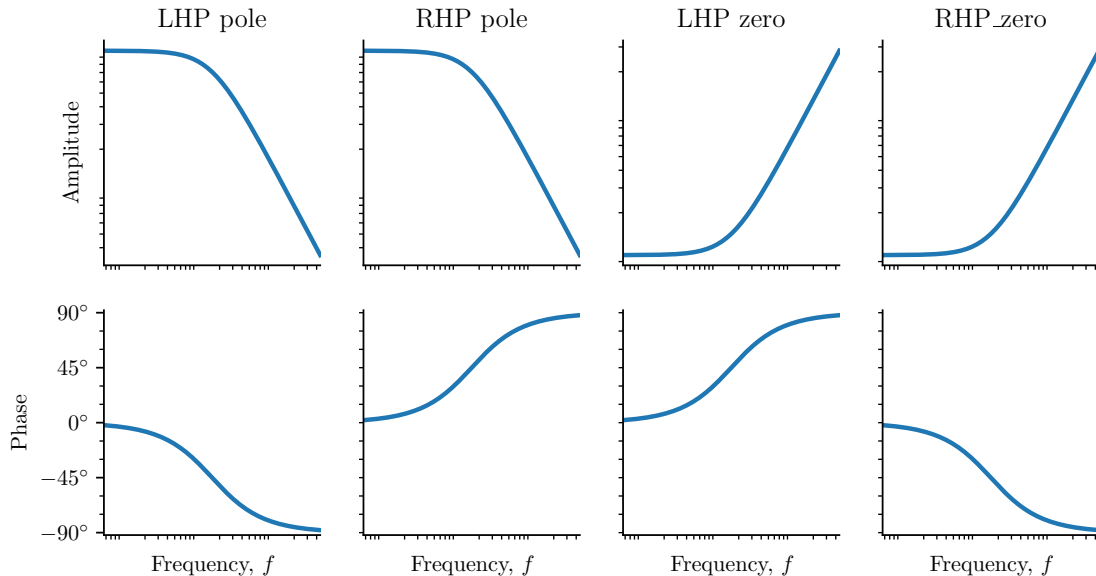
Also, if  $\tilde{g}(0)$  is finite and nonzero, we usually prefer to write

$$\tilde{g}(s) = \tilde{g}(0) \frac{(1 - s/z_0)(1 - s/z_1)(1 - s/z_2) \cdots}{(1 - s/p_0)(1 - s/p_1)(1 - s/p_2) \cdots}$$

where

$$\tilde{g}(0) = k \times \frac{\prod_i p_i}{\prod_i z_i}$$

# Taxonomy of poles and zeros





# ZPK representation of the damped harmonic oscillator

For the damped harmonic oscillator:

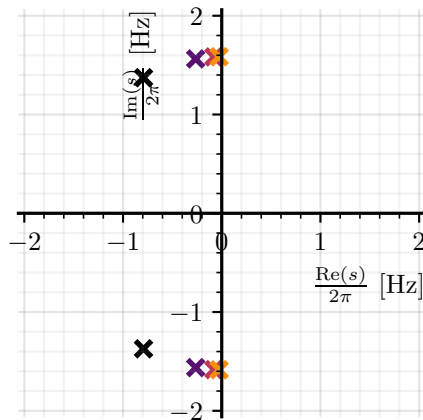
$$\frac{\tilde{x}(s)}{\tilde{F}(s)} = \frac{1/m}{(s - p_+)(s - p_-)}$$

where  $p_{\pm} = -\frac{\Omega_0}{2Q} (1 \pm i\sqrt{4Q^2 - 1})$ .

Note

- $|p_{\pm}| = \Omega_0$
- $\arg p_{\pm} = \arccos(1/2Q)$ .

For  $Q \gg 1$ ,  $p_{\pm} \approx -\Omega_0(1/2Q \pm i)$ .



## Exercise: Bode plots of some LTI systems

By hand, sketch a Bode plot (i.e., the amplitude and phase) of the frequency response for some or all of the following cases:

- 1 A real pole at  $s = -2\pi \times 10 \text{ Hz}$  and a real zero at  $s = -2\pi \times 100 \text{ Hz}$ , with a gain of 1 at ac ( $f = \infty \text{ Hz}$ ).
- 2 A real pole at  $s = -2\pi \times 100 \text{ Hz}$  and a real zero at  $s = +2\pi \times 100 \text{ Hz}$ , with a gain of 1 at dc ( $f = 0 \text{ Hz}$ ).
- 3 (Challenge) A complex pair of poles at  $s = 2\pi \times (-0.1 \text{ Hz} \pm 10i \text{ Hz})$ , a real pole at  $s = 2\pi \times 0 \text{ Hz}$ , and a real zero at  $s = -2\pi \times 10 \text{ Hz}$ , with a gain of 1 at 100 Hz.

Draw your Bode plots with the horizontal axis in ordinary frequency  $f = \Omega/2\pi = s/2\pi i$ .

Without a calculator, estimate the phase of the frequency responses at  $f = 10 \text{ Hz}$ ,  $f = 100 \text{ Hz}$ , and  $f = 1000 \text{ Hz}$ .

# Measuring the frequency response

A frequency response is also known as a **transfer function** or **input–output relation** or **scattering matrix**.

Taking the example  $\tilde{x}(f)/\tilde{F}(f)$ , the transfer function is measured at each frequency  $f_j = \Omega_j/2\pi$  by:

- Injecting a sine wave  $F_j \sin(\Omega_j t)$
- Recording the sinusoidal response  $x_j \sin(\Omega_j t + \phi_j) + n(t)$ , which has random noise  $n$

The transfer function at that frequency is the complex number  $(x_j/F_j)e^{-i\phi_j}$ .

# Linear, time-invariant systems (LTI)

It turns out the systems we have dealt with so far are **linear** (two solutions can always be superposed to make a third valid solution) and **time invariant** (time delaying the input simply time delays the output).

Any such system is completely characterized by its frequency response, and has the property that a sine wave at the input always produces a sine wave at the output, although it may be phase delayed.

# Impulse response

If  $\tilde{H}(s)$  is a frequency response, then the inverse Laplace transform  $H(t) \xleftarrow{\mathcal{L}^{-1}} \tilde{H}(s)$  defines the **impulse response** of the system.

The name is literal: it is the system's time-domain response to a quick, pulse-like force.



Bruel & Kjaer impact hammer

# Stability: poles in the left or right half-plane

A system is **stable** if and only if **all poles in the system have negative real part** (“left half-plane”). A perturbation to the system decays to zero as  $t \rightarrow \infty$ .

If **any pole has a positive real part** (“right half-plane”), the impulse response diverges as  $t \rightarrow \infty$ . The system is **unstable**.

